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Brief paper Distance function design and Lyapunov techniques for the stability of hybrid trajectories^{*}



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ABSTRACT

The comparison between time-varying hybrid trajectories is crucial for tracking, observer design and synchronisation problems for hybrid systems with state-triggered jumps. In this paper, a generic distance function is designed that can be used for this purpose. The so-called "peaking phenomenon", which occurs when using the Euclidean distance to compare two hybrid trajectories, is circumvented by taking the hybrid nature of the system explicitly into account. Based on the proposed distance function, we define the stability of a trajectory and present sufficient Lyapunov-type conditions for hybrid systems with state-triggered jumps. A constructive Lyapunov function design is presented for hybrid systems with affine flow and jump maps and a jump set that is a hyperplane. The stability conditions can then be verified using linear matrix conditions. Finally, for this class of systems, we present a tracking controller that asymptotically stabilises a given hybrid reference trajectory and we illustrate our results with an example. © 2016 Elsevier Ltd. All rights reserved.

1. Introduction

Hybrid system models have proven valuable to capture the dynamics of complex systems arising in engineering, biological, and economical systems as these models combine continuous-time dynamics with discrete events or jumps (Goebel, Sanfelice, & Teel, 2012; Heemels, de Schutter, Lunze, & Lazar, 2010). While the stability of isolated points or closed sets of hybrid systems is relatively well-understood (Goebel et al., 2012; Heemels et al., 2010), the stability of time-varying trajectories received significantly less attention and many issues are presently unsolved. Given the importance

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http://dx.doi.org/10.1016/j.automatica.2016.07.006 0005-1098/© 2016 Elsevier Ltd. All rights reserved. of stability of trajectories in tracking control, observer design and synchronisation problems, it is important to address these open issues.

One of the main complications to study the stability of hybrid trajectories is the "peaking phenomenon" of the Euclidean distance between two trajectories, that can be observed when jump times do not coincide, and the states of two hybrid trajectories are compared at the same continuous-time instant, cf. Biemond, van de Wouw, Heemels, and Nijmeijer (2013), Leine and van de Wouw (2008), Menini and Tornambè (2001) and Sanfelice, Biemond, van de Wouw, and Heemels (2014). Focussing on mechanical systems with unilateral position constraints, the 'peaking phenomenon' has motivated the Zhuravlev-Ivanov method, cf. Brogliato (1999) and related method of Forni, Teel, and Zaccarian (2013), in which tracking control and observer problems are defined by requiring the asymptotic stability of a set that consists of the real system and 'mirrored' images. For impacting mechanical systems, in Galeani, Menini, Potini, and Tornambè (2008), Menini and Tornambè (2001) and Morărescu and Brogliato (2010), the standard Euclidean state error is employed away from the impacts times, while near impacts, only the position error, and no velocity error is considered.



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Alternatively, measures on complete trajectories are presented in Broucke and Arapostathis (2002) and Goebel et al. (2012).

To effectively address stability problems for a large class of hybrid systems, we aim to express stability in terms of a distance function evaluated along trajectories. In Biemond et al. (2013), this is facilitated by a distance function that takes the jumping nature of the hybrid system into account, therewith avoiding the "peaking phenomenon". For this purpose, a distance function between two states is used which is zero if either both states are equal, or they can become identical after imminent jumps. We note that this implies that the functions considered do not satisfy the conditions to be a metric. However, no constructive design for this distance function was presented in Biemond et al. (2013). Focussing on a class of constrained mechanical systems, a similar distance function was employed in Schatzman (1998) to study continuity of trajectories with respect to initial conditions. In both works, adhoc techniques were used to design the distance function.

As a first contribution in the current paper, we present a constructive and general design for the distance function. We show that when (global) asymptotic stability is defined with respect to the new distance function, then the proposed distance function provides an intuitively correct comparison between two hybrid trajectories. Subsequently, sufficient conditions for asymptotic stability are presented that rely on Lyapunov functions that may increase during either flow or jump, as long as the Lyapunov function eventually decreases along solutions. For this purpose, maximal or minimal average dwell-time arguments are employed, as proposed in the context of impulsive systems in Hespanha, Liberzon, and Teel (2008). The final contribution consists of the application of the developed stability theory to tracking control problems for a class of hybrid systems where the jump map is an affine function of the state, the jump set is a hyperplane, and the continuous-time dynamics can be influenced by a bounded control input. A piecewise affine tracking control law is designed that achieves asymptotic tracking in the proposed distance measure. Finally, the results of this paper are illustrated with an example. Preliminary results have been advertised in Biemond, Heemels, Sanfelice, and van de Wouw (2015).

This paper is outlined as follows. We present the class of hybrid systems considered in Section 2. By presenting the constructive distance function design, in Section 3, stability of trajectories is defined and a Lyapunov theorem is formulated. A constructive piecewise quadratic Lyapunov function is designed in Section 4 for a class of hybrid systems with affine jump maps and the jump set contained in a hyperplane. These results are applied to tracking control problems in Section 5. Finally, an example is given in Section 6, followed by conclusions in Section 7.

Notation: Let \mathbb{N} and $\mathbb{N}_{>0}$ denote the set of nonnegative and positive integers, respectively. For a set $X \subset \mathbb{R}^n$, ∂X denotes its boundary and for each $y \in \mathbb{R}^n$, the distance between y and X is $dist(y, X) := inf_{x \in X} ||x - y||$. The set $\mathbb{B} \subset \mathbb{R}^n$ is the closed unit ball. Given $x \in \mathbb{R}^n$, $y \in \mathbb{R}^m$, let (x, y) denote $(x^T, y^T)^T$. Given a (possibly set-valued) map *F* with domain of definition dom $F \subset \mathbb{R}^n$ and a set $S \subseteq \text{dom } F, F(S) = \{y \mid y \in F(x), \text{ with } x \in S\}$ denotes its image; $F(y) = \emptyset$ for $y \notin \text{dom } F$, $F^k(x)$, with $x \in \mathbb{R}^n$, $k \in \mathbb{N}_{>0}$, denotes $F(F^{k-1}(x))$ and for all $x \in \mathbb{R}^n$, $F^0(x) = \{x\}$. We denote the pre-image as $F^{-1}(S) = \{x \mid F(x) \cap S \neq \emptyset\}$. A set-valued map $F : S \subset \mathbb{R}^n \Rightarrow \mathbb{R}^n$ is outer semicontinuous if its graph $\{(x, y) \in \mathbb{R}^n \times \mathbb{R}^n \mid x \in S, y \in F(x)\}$ is closed, and locally bounded if, for each compact set $\tilde{S} \subseteq S$, $F(\tilde{S})$ is bounded. For $n, m \in \mathbb{N}_{>0}$, let I_n and O_{mn} denote the identity matrix and the matrix of zeros of dimension $n \times n$ and $m \times n$, respectively. Given matrices $A, B \in \mathbb{R}^{n \times n}, A \prec 0$ and $A \preceq 0$ denote that A is symmetric and negative definite or negative semidefinite, respectively.

2. Hybrid system model

Consider the hybrid system

$$\dot{x} \in F(t, x) \quad x \in C,$$
 (1a)

$$x^+ \in G(x) \quad x \in D, \tag{1b}$$

with $F : [t_0, \infty) \times C \Rightarrow \mathbb{R}^n$ and $G : D \Rightarrow \mathbb{R}^n$, where $C \subseteq \mathbb{R}^n$ and $D \subseteq \mathbb{R}^n$. We emphasise that the jump map *G* is independent of the time *t*, which, in the following, will be exploited in the design of the distance function. In contrast to embedding an extra variable with dynamics $\dot{t} = 1$, we prefer to use explicit time-dependency of the flow map *F*, as this allows to study the perturbation of initial conditions without perturbing the initial time. The class of hybrid systems in the form (1) is quite general and permits to model systems arising in many relevant applications, including mechanical systems with impacts (Goebel et al., 2012) and event-triggered control systems, see e.g. Postoyan, Tabuada, Nesic, and Anta (2015). We consider systems (1) that satisfy the following "hybrid basic conditions" (adapted to allow for non-autonomous flow maps).

Assumption 1. The data of the hybrid system satisfies

- *C*, *D* are closed subsets of \mathbb{R}^n with $C \cup D \neq \emptyset$;
- the set-valued mapping F(t, x) is non-empty for all $(t, x) \in [t_0, \infty) \times C$, measurable, and for each bounded closed set $S \subset [t_0, \infty) \times C$, there exists an almost everywhere finite function m(t) such that $||f|| \leq m(t)$ holds for all $f \in F(t, x)$ and for almost all $(t, x) \in S$;
- $G : D \Rightarrow \mathbb{R}^n$ is nonempty, outer semicontinuous and locally bounded.

We consider solutions φ to (1) defined on a hybrid time domain dom $\varphi \subset [t_0, \infty) \times \mathbb{N}$ as given in Goebel et al. (2012). The function φ : dom $\varphi \mapsto \mathbb{R}^n$ is a solution of (1) when jumps satisfy (1b) and, for fixed $j \in \mathbb{N}$, the function $t \mapsto \varphi(t, j)$ is locally absolutely continuous in t and a Krasovskii solution to (1a). This means $\varphi(t,j) \in D$ and $\varphi(t,j+1) \in G(\varphi(t,j))$ for all $(t,j) \in \operatorname{dom} \varphi$ such that $(t, j + 1) \in \operatorname{dom} \varphi$ and $\varphi(t, j) \in C$, $\frac{d}{dt}\varphi(t, j) \in \overline{F}(t, \varphi(t, j))$ for almost all $t \in I_j := \{t \mid (t, j) \in \operatorname{dom} \varphi\}$ and all j such that I_j has nonempty interior. Herein, $\overline{F}(t, x) = \bigcap_{\delta > 0} \operatorname{co}\{F(t, (x + \delta \mathbb{B}) \cap C)\}$ and co denotes the closed convex hull operation. We note that this convexification renders $\overline{F}(t, x)$, when restricted to a bounded closed set S, convex, outer semi-continuous and measurable in t, such that solutions to the differential equation can be defined, cf. Filippov (1988, Theorem 6, p. 86). The solution φ is said to be maximal if it cannot be extended, complete if dom φ is unbounded, and dom φ is called unbounded in *t*-direction when for each $T \geq t_0$ there exists a *j* such that $(T, j) \in \text{dom } \varphi$.

3. Design of distance function and stability notion

We restrict our attention to hybrid systems satisfying the following assumption.

Assumption 2. The data of the hybrid system (1) is such that *G* is a proper function (cf. Definition 1.4.11 in Aubin & Frankowska, 2009), there is a k > 0 for which $G^k(D) \cap D = \emptyset$ and every maximal solution of (1) has a hybrid time domain that is unbounded in *t*-direction.

This assumption implies that neither Zeno behaviour nor finitetime escape of solutions is possible. **Definition 1.** Consider the hybrid system (1) satisfying Assumption 1 and let $\bar{k} > 0$ denote the minimum integer for which Assumption 2 holds. Let the distance function $d : (C \cup D)^2 \mapsto \mathbb{R}_{\geq 0}$ be defined by

$$d(x, y) = \inf_{z \in \mathcal{A}} \|(x, y) - z\|$$
(2)

with

$$\mathcal{A} := \left\{ (z_x, z_y) \in (C \cup D)^2 \middle| \exists k_1, k_2 \in \{0, 1, \dots, \bar{k}\}, G^{k_1}(z_x) \cap G^{k_2}(z_y) \neq \emptyset \right\}.$$
(3)

The following theorem summarises particular properties of the distance function *d*.

Theorem 1. Consider the hybrid system (1) satisfying Assumption 1 and let \bar{k} denote the minimum integer for which Assumption 2 holds. The set A in (3) is closed and the function d in Definition 1 is continuous and satisfies

- (1) d(x, y) = 0 if and only if there exist $k_1, k_2 \in \{0, 1, \dots, \bar{k}\}$ such that $G^{k_1}(x) \cap G^{k_2}(y) \neq \emptyset$,
- (2) { $y \in C \cup D \mid d(x, y) < \beta$ } is bounded for all $x \in C \cup D$, and all $\beta > 0$, and
- (3) d(x, y) = d(y, x), for all $x, y \in C \cup D$.

Proof. In order to prove (1), we prove that the infimum in (2) is always attained. First, we observe from Assumption 1 that *G* is outer semicontinuous, which directly implies that G^{-1} is outer semicontinuous. In addition, as *G* is proper according to Assumption 2, we observe that G^{-1} is locally bounded, cf. Aubin and Frankowska (2009).

Since the composition $M_1 \circ M_2$ of set-valued mappings M_1 and M_2 is outer semicontinuous and locally bounded when M_1 and M_2 are outer semicontinuous and locally bounded, we observe that G^{k_2} is outer semicontinuous and locally bounded for all $k_2 \in \{0, 1, \ldots, \bar{k}\}$. In addition, reusing this argument, $G^{-k_1}G^{k_2}$ is outer semicontinuous and locally bounded for all $k_1, k_2 \in \{0, 1, \ldots, \bar{k}\}$.

Note that $\mathcal{A} = \bigcup_{k_1,k_2 \in \{0,1,\ldots,\bar{k}\}} A_{k_1k_2}$, with $A_{k_1k_2} := \{(x,y) \in (C \cup D)^2 \mid y \in G^{-k_1}G^{k_2}(x)\}$, cf. (3). As, for all $k_1, k_2 \in \{0, 1, \ldots, \bar{k}\}$, $G^{-k_1}G^{k_2}$ is outer semicontinuous and locally bounded, and $(C \cup D)^2$ is closed, we conclude that each set $A_{k_1k_2}$ is closed. Consequently, we find that the functions $d_{k_1k_2}(x, y) := \text{dist}((x, y), A_{k_1k_2})$, for each $k_1, k_2 \in \{0, 1, \ldots, \bar{k}\}$, are either continuous functions, or, when $A_{k_1k_2} = \emptyset$, identical to infinity. Since A_{00} is nonempty, we observe that $d_{00}(x, y)$ is a continuous and locally bounded function in $C \cup D$. We may write $d(x, y) = \min_{k_1,k_2 \in \{0, 1, \ldots, \bar{k}\}} d_{k_1k_2}(x, y)$, proving that d is continuous. As each set $A_{k_1k_2}$ is closed, \mathcal{A} is closed, such that d(x, y) = 0 if and only if $(x, y) \in \mathcal{A}$, proving (1).

We now prove (2) by showing that, for every $x \in C \cup D$,

$$Y_{\infty}(x) := \{ y \in C \cup D \mid \exists (z_x, z_y) \in \mathcal{A}, \\ \|x - z_x\| \le \beta, \ \|y - z_y\| \le \beta \}$$

$$(4)$$

is bounded for $\beta > 0$. For any x, the set $X_{\beta}^{0} := \{w_{x} \mid ||w_{x} - x|| \le \beta\}$ is compact. Since we have shown above that $G^{-k_{1}}G^{k_{2}}$ is outer semicontinuous and locally bounded for all $k_{1}, k_{2} \in \{0, 1, \ldots, \bar{k}\}$, we find that the set $G^{-k_{1}}G^{k_{2}}(X_{\beta}^{0})$ is compact for all $k_{1}, k_{2} \in \{0, 1, \ldots, \bar{k}\}$. As z_{y} in (4) has to satisfy $z_{y} \in G^{-k_{2}}G^{k_{1}}(X_{\beta}^{0})$ for some $k_{1}, k_{2} \in \{0, 1, \ldots, \bar{k}\}$, we have shown that z_{y} is contained in a bounded set. Hence, we observe that $Y_{\infty}(x)$ is bounded, which implies (2). Property (3) directly follows from symmetry of (3), which completes the proof. \Box

Remark 1. Note that the function d in (2) is not a metric, as it does not satisfy the triangle inequality. Namely, if *G* is set-valued and, for some *x*, *G*(*x*) contains two distinct points *y* and *z*, then d(x, y) = 0

and d(x, z) = 0 by Definition 1, while $d(y, z) \neq 0$ may still hold in many cases.

An alternative distance function design is presented in Appendix A, which has the advantage that, evaluated along solutions, it yields a continuous function in time. We prefer (2) due to its more simple formulation.

In order to enable the comparison of the states of two trajectories in terms of the distance *d*, similar to Biemond et al. (2013), we introduce the extended hybrid system with state $q = (x, y) \in (C \cup D)^2$, flow map

$$\dot{q} \in F_e(t,q) := (F(t,x), F(t,y)), \tag{5a}$$

for $(x, y) \in C_e := C^2$ and jumps characterised by

$$q^{+} = G_{e}(q) := \begin{cases} (G(x), y) & \text{if } x \in D, y \in C \setminus D \\ (x, G(y)) & \text{if } x \in C \setminus D, y \in D \\ \{(G(x), y), (x, G(y))\} & \text{if } x, y \in D \end{cases}$$
for $a \in D$, $i \in [(x, y) \in (C + D)^{2} + y \in D) (y \in D)$

$$(5b)$$

for $q \in D_e := \left\{ (x, y) \in (C \cup D)^2 \mid x \in D \lor y \in D \right\}$ (5b)

and select the initial condition $(\varphi_x(t_0, 0), \varphi_y(t_0, 0)) = \varphi_q(t_0, 0)$. We note that the set-valued function G_e above motivated the design of the set A in (3), cf. Biemond et al. (2013). Namely, A represents the smallest set that contains all points (x, y) with x = y that can be forward invariant under (5).

Solutions of this extended system generate a combined hybrid time domain. Introducing $\bar{\varphi}_x(t,j) := (I_n \quad O_{nn}) \varphi_q(t,j)$, and $\bar{\varphi}_y(t,j) := (O_{nn} \quad I_n) \varphi_q(t,j)$, hence allows to evaluate the distance $d(\bar{\varphi}_x(t,j), \bar{\varphi}_y(t,j))$ at every time instant $(t,j) \in \text{dom } \varphi_q$.

Given a trajectory φ_x of (1), we say that a trajectory $(\bar{\varphi}_x, \bar{\varphi}_y)$ of (5) represents φ_x in the first *n* states when $\bar{\varphi}_x$ is a reparameterisation of φ_x . Clearly, any trajectory to (5) represents φ_x in the first *n* states when $\bar{\varphi}_x(t_0, 0) = \varphi_x(t_0, 0)$ holds and from this initial condition system (1) has a unique solution, as considered in Biemond et al. (2013).

Definition 2. Consider a hybrid system (1) satisfying Assumption 2 and let *d* be given in (2). The trajectory φ_x of (1) is called *stable* with respect to *d* if for all $\epsilon > 0$ there exists a $\delta(\epsilon) > 0$ such that for every initial condition $\varphi_y(t_0, 0)$ satisfying $d(\varphi_x(t_0, 0), \varphi_y(t_0, 0)) \le \delta(\epsilon)$, it holds that

$$d(\bar{\varphi}_{x}(t,j),\bar{\varphi}_{y}(t,j)) < \epsilon \quad \text{for all } (t,j) \in \text{dom } \varphi_{q}, \tag{6}$$

with $\varphi_q(t, j) = (\bar{\varphi}_x(t, j), \bar{\varphi}_y(t, j))$ being any maximal solution to (5) with initial condition ($\varphi_x(t_0, 0), \varphi_y(t_0, 0)$) that represents φ_x in the first *n* states, and is called *asymptotically stable with respect to d* if δ can be selected such that, in addition,

$$\lim_{t+j\to\infty} d(\bar{\varphi}_{x}(t,j),\bar{\varphi}_{y}(t,j)) = 0.$$
(7)

When the trajectory φ_x is asymptotically stable with respect to d and (7) holds for all maximal solutions φ_q to (5), then the trajectory φ_x is called globally asymptotically stable with respect to d.

Remark 2. This stability notion is more general than stability of the set A in (3) for system (5), since initial conditions of φ_q in (5) are restricted to $\bar{\varphi}_x(t_0, 0) = \varphi_x(t_0, 0)$.

To analyse stability using Lyapunov functions that may increase during flow and decrease during jumps, or vice versa, minimal and maximal average inter-jump time are considered as follows.

Definition 3 (*Hespanha et al., 2008*). A hybrid time domain *E* is said to have minimal average inter-jump time $\tau > 0$ if there exists $N_0 > 0$ such that for all $(t, j) \in E$ and all $(T, J) \in E$ where $T + J \ge t + j$, it holds that $J - j \le N_0 + \frac{T-t}{\tau}$.

A hybrid time domain *E* is said to have maximal average interjump time $\tau > 0$, if there exists $N_0 > 0$ such that for all $(t, j) \in E$ and all $(T, J) \in E$ where $T + J \ge t + j$, it holds that $J - j \ge \frac{T - t}{\tau} - N_0$.

We say that a hybrid trajectory φ_q has a minimal or maximal average inter-jump time if dom φ_q has a minimal or maximal average inter-jump time, respectively.

The following theorem presents Lyapunov-based sufficient conditions for the stability of a trajectory φ_x of (1). As we are interested in stability for given φ_x , these conditions are imposed only near this trajectory.

Theorem 2. Consider a hybrid system (1) satisfying Assumptions 1 and 2. Let d be given in (2). The trajectory φ_x of system (1) is asymptotically stable with respect to d if there exist a continuous function $V : \mathbb{R}^n \times \mathbb{R}^n \mapsto \mathbb{R}_{\geq 0}$, \mathcal{K}_{∞} -functions α_1, α_2 , a scalar $v_L > 0$ and scalars λ_c , λ_d such that V is continuously differentiable on an open domain containing $V_L := V^{-1}([0, v_L])$ and, for all $(t, j) \in$ dom φ_x , it holds that

$$\alpha_1(d(\varphi_x(t,j),y)) \le V(\varphi_x(t,j),y) \le \alpha_2(d(\varphi_x(t,j),y)),$$

for all y such that $(\varphi_x(t,j),y) \in C_e \cup D_e,$ (8)

$$V(g) \le e^{\lambda_d} V(q), \text{ for all } g \in G_e(q),$$

and all y such that $q = (\varphi_x(t, j), y) \in D_e \cap V_L,$ (9)

$$\left(\frac{\partial V}{\partial q}\Big|_{q}, f\right) \leq \lambda_{c} V(\varphi_{x}(t, j), y) \quad \text{for all } f \in \bar{F}_{e}(t, q)$$

and all y such that $q = (\varphi_{x}(t, j), y) \in C_{e} \cap V_{L},$ (10)

and at least one of the following conditions are satisfied:

- (1) $\lambda_c < 0, \lambda_d \le 0$;
- (2) all trajectories of (1) have minimal average inter-jump time $2\tau > 0$, $\lambda_c \leq 0$ and $\lambda_d + \lambda_c \tau < 0$;
- (3) all trajectories of (1) have maximal average inter-jump time $2\tau > 0, \lambda_d \leq 0$ and $\lambda_d + \lambda_c \tau < 0$.

When, in addition, (9) and (10) hold for all y such that $q = (\varphi_x(t, j), y) \in D_e$ and C_e , respectively, then φ_x is globally asymptotically stable with respect to d.

Proof. The proof is given in Appendix B. \Box

Remark 3. The dependency of *V* on the trajectory $\varphi_x(t, j)$ implies that *V* in Theorem 2 takes the role of a (hybrid) time-dependent Lyapunov function $v(t, j, y) = V(\varphi_x(t, j), y)$, with $(t, j) \in \text{dom } \varphi_x$. In this manner, v(t, j, y) characterises the distance $d(y, \varphi_x(t, j))$ between φ_x at (t, j) and *y*.

The conditions (8)-(10) are closely related to the Lyapunov conditions used for incremental stability, see e.g. Angeli (2002) and Rüffer, van de Wouw, and Mueller (2013) for ordinary differential equations and Li, Phillips, and Sanfelice (2016) for hybrid systems where incremental stability is defined with respect to the Euclidean distance, and Zamani, van de Wouw, and Majumdar (2013) where incremental stability with respect to non-Euclidean distance functions is investigated for ordinary differential equations. In fact, if the conditions of Theorem 2 hold for *any* solution $\varphi_x(t, j)$ of (1), then they imply asymptotic stability of the set A of system (5) and, equivalently, an incremental stability property of (1) with respect to the distance d. However, as mentioned above, those conditions need to be satisfied for all φ_x , which makes them stringent and our result relaxes this by requiring (8)–(10) to hold for each point in the range of φ_x only. Consequently, the conditions in Theorem 2 are less restrictive than the conditions for stability of the set A obtained using the results of Goebel et al. (2012).

In fact, the stability of the trajectory φ_x considered in Theorem 2 is *less restrictive* than stability of the set \mathcal{A} for the dynamics (5)

(or, equivalently, incremental stability of (1)), since the particular trajectory φ_x is known.

4. Constructive Lyapunov function design for hybrid systems with affine jump map

In this section we present the design conditions for the construction of a piecewise quadratic Lyapunov function that, locally, satisfies the requirements (8) and (9). To be able to write the stability conditions in terms of Linear Matrix Inequalities, we need to focus on a class of "linear" hybrid systems: in particular, having single-valued, affine and invertible jump maps and jump sets characterised by a hyperplane as follows:

$$\dot{x} = f(t, x), \quad x \in C, \tag{11a}$$

$$x^+ = Lx + H, \quad x \in D \tag{11b}$$

with the function f measurable in its first argument and Lipschitz in its second argument, the matrix $L \in \mathbb{R}^{n \times n}$ being invertible, and $H \in \mathbb{R}^n$. Furthermore, the sets C and D are nonempty, closed and satisfy

$$C \subseteq \{x \in \mathbb{R}^n \mid Jx + K \le 0 \land$$

($IL^{-1}x + K - IL^{-1}H$)s < 0 $\}.$ (11c)

$$D := \{x \in C \mid Jx + K = 0 \land z_1 x + z_2 \le 0\},$$
(11d)

where the parameters J^T , $z_1^T \in \mathbb{R}^n \setminus \{0\}$, K, $z_2 \in \mathbb{R}$ characterise the half hyperplane containing D, and $s \in \{-1, 1\}$ is selected such that $n_{gd} := s(L^{-1})^T J^T$ is a normal vector to G(D) pointing out of C. Let $G(D) \subset C$ and the following assumption hold.

Assumption 3. The data of (11) is such that there exist scalars $z_3, z_4, z_5 > 0$ such that

- $z_1x + z_2 \ge z_3$ for all $x \in G(D)$,
- $Jx + K < -z_4$ for all $x \in C$ that satisfy $|z_1x + z_2| \le z_3$,
- for all $x \in C$ with $z_1x + z_2 \leq 0$, there exists a $y \in D$ such that $Jx + K \leq -z_5 ||x y||$,
- all maximal solutions of (11) are complete.

The first three bullets of this assumption are illustrated in Fig. 1. Note that this assumption directly implies $D \cap G(D) = \emptyset$, cf. Assumption 2. All solutions to (11) have a time domain that is unbounded in *t*-direction, as, firstly, $G(D) \cap D = \emptyset$ excludes Zenobehaviour since *D* is closed, secondly, *G* is linear and, thirdly, *f* is Lipschitz in its second argument. Hence, Assumption 3 implies that Assumptions 1 and 2 hold for system (11). In Section 6, we present an example of a mechanical system that satisfies (11) and Assumption 3.

In order to present a constructive Lyapunov function design, we first introduce the function $\overline{G} : \mathbb{R}^n \mapsto \mathbb{R}^n$ as

$$\bar{G}(x) := Lx + H + M(Jx + K) + sLJ^T \max(0, z_1x + z_2),$$
(12)

where the parameter $M \in \mathbb{R}^n$ is to be designed. Note that if $x \in D$, then $\overline{G}(x) = G(x) = Lx + H$.

Since $G(D) \cap D = \emptyset$, Definition 1 implies that d(x, y) = 0 if and only if x = y, or x = G(y), or y = G(x). To design a Lyapunov function *V*, we note that (8) requires that V(x, y) = 0 if and only if d(x, y) = 0. Hence, we propose the following piecewise quadratic Lyapunov function:

$$V(x, y) = \min(\|x - y\|_{P_0}^2, \|x - \bar{G}(y)\|_{P_s}^2, \|\bar{G}(x) - y\|_{P_s}^2),$$
(13)

where the positive definite matrices $P_0, P_s \in \mathbb{R}^{n \times n}$ are to be designed. While this function is not smooth, we restrict our attention to a sufficiently small sub-level set where, as we will show in Lemma 3, the function *V* is smooth.



Fig. 1. Pictorial illustration of the phase space of (11) when Assumption 3 is satisfied. The second and third bullets of this assumption imply that the intersection between *C* and the domains depicted in dark grey and light grey, respectively, is empty.

Design of Lyapunov function parameters

To design the parameters P_0 , P_s and M of the Lyapunov function V in (13), we employ the following lemma.

Lemma 3. Consider the hybrid system (11), let $M \in \mathbb{R}^n$ satisfy $(JL^{-1}M + 1)s < 0$, let $P_0, P_s > 0$ and let Assumption 3 hold. Consider the function V in (13). If for some $\lambda_d \in \mathbb{R}$ it holds that

$$(L+MJ)^T P_s(L+MJ) \leq e^{\lambda_d} P_0, \tag{14}$$

$$P_0 \leq e^{\lambda_d} P_s, \tag{15}$$

then there exist \mathcal{K}_{∞} -functions α_1, α_2 and $v_L > 0$ such that the conditions (8) and (9) in Theorem 2 are satisfied with $V_L = V^{-1}([0, v_L])$ and the function V in (13) is smooth on an open domain containing V_L .

Proof. The proof is given in Appendix B. \Box

This lemma provides sufficient conditions on the hybrid systems (11) and the Lyapunov function (13) such that the conditions (8) and (9) are satisfied. In the following section, we present a tracking control law, and additional conditions on *V*, such that the other conditions in Theorem 2 are also satisfied.

5. Tracking control problems

We now employ the results on the asymptotic stability of jumping hybrid trajectories to solve a tracking problem of a hybrid trajectory with jumps.

We restrict our attention to tracking control problems for the class of systems (11) with $f(t, x) = Ax + E + Bu(t, x), A \in \mathbb{R}^{n \times n}$, $E, B \in \mathbb{R}^n$, with a control law $u : [0, \infty) \times C \mapsto \mathbb{R}$ to be designed. In the scope of this tracking problem, we consider a reference trajectory x_d , which is a solution to (11) for a feedforward input signal $u(t, x) = u_{\rm ff}(t)$. We assume that y is a trajectory that is generated by the control signal $u(t, y) = u_{\rm ff}(t) + u_{\rm fb}(t, y)$, and assume that $u_{\rm fb}$ vanishes along the trajectory x_d , i.e. $u_{\rm fb}(t, x_d(t, j)) = 0$ for almost all $(t, j) \in \text{dom } x_d$ (appropriate designs for $u_{\rm fb}$ will depend on the known trajectory x_d). Hence, the flow map of the extended hybrid system (5) is given by

$$F_e(t, x_d, y) = \begin{pmatrix} Ax_d + E + B(u_{\rm ff}(t) + u_{\rm fb}(t, x_d)) \\ Ay + E + B(u_{\rm ff}(t) + u_{\rm fb}(t, y)) \end{pmatrix}.$$
 (16)

We partition $C_e \cup D_e$ in the three sets S_0 , S_1 , S_2 where the minimiser of (13) is $||x - y||_{P_0}^2$, $||x - \overline{G}(y)||_{P_s}^2$ or $||\overline{G}(x) - y||_{P_s}^2$, respectively.

Introducing the function $\bar{x}_d(t) := x_d(t, \min_{(t,j) \in \text{dom } x_d} j)$, we design a switching feedback law u_{fb} as:

$$u_{\rm fb}(t,y) = \begin{cases} -c_0(x_d(t) - y), \\ \text{for } (\bar{x}_d(t), y) \in S_0 \\ -\frac{\beta_2^T}{\beta_2^T} \beta_1(t) - c_1(\bar{x}_d(t) - \bar{G}(y)), \\ \text{for } (\bar{x}_d(t), y) \in S_1 \\ -\frac{\beta_4^T}{\beta_4^T} \beta_3(t) - c_2(\bar{G}(\bar{x}_d(t)) - y), \\ \text{for } (\bar{x}_d(t), y) \in S_2 \end{cases}$$
(17)

with $c_0^T, c_1^T, c_2^T \in \mathbb{R}^n$,

$$\begin{split} \beta_1(t) &= \begin{pmatrix} I_n & -L - MJ \end{pmatrix} \begin{pmatrix} A\bar{x}_d(t) + Bu_{\rm ff}(t) + E \\ A\bar{G}^\circ(\bar{x}_d(t)) + Bu_{\rm ff}(t) + E \end{pmatrix}, \\ \beta_3(t) &= \begin{pmatrix} L + MJ & -I_n \end{pmatrix} \begin{pmatrix} A\bar{x}_d(t) + Bu_{\rm ff}(t) + E \\ A\bar{G}(\bar{x}_d(t)) + Bu_{\rm ff}(t) + E \end{pmatrix}, \end{split}$$

 $\beta_2 = -(L + MJ)B$ and $\beta_4 = -B$, where $\overline{G}^{\circ}(x)$ is designed as $\overline{G}^{\circ}(x) = (L + MJ)^{-1}(x - H - MK)$, which, restricted to $S_1 \cap V_L$, coincides with the inverse of \overline{G} .

Using this switched control law, which switches on the basis of the Lyapunov function designed in (13), we formulate in the following result explicit conditions on the controller parameters c_0 , c_1 , c_2 , M, P_0 and P_s under which the tracking problem is solved.

Theorem 4. Consider the hybrid system (11) with $f(t, x) = Ax + E + B(u_{\rm ff}(t) + u_{\rm fb}(t, x))$, for some measurable function $u_{\rm ff}(t)$ and let x_d be a solution of (11) for $u_{\rm fb} \equiv 0$. Let $P_0, P_s \in \mathbb{R}^{n \times n}, M \in \mathbb{R}^n$, consider V as in (13) and let $u_{\rm fb}$ be designed as in (17), with $\bar{x}_d(t) = x_d(t, \min_{(t,j) \in dom x_d} j)$ and $c_0^T, c_1^T, c_2^T \in \mathbb{R}^n$. Let L + MJ be invertible and $B \neq 0$.

Let the assumptions of Lemma 3 hold for $\lambda_d \in \mathbb{R}$, let all trajectories of (11) have a time domain that is unbounded in t-direction, and assume

$$\beta_1(t) \in span(\beta_2), \quad and \quad \beta_3(t) \in span(\beta_4)$$
 (18)

hold for almost all t.

Let, for some $\lambda_c \in \mathbb{R}$, the following LMIs be satisfied:

$$(A + Bc_0)^{I} P_0 + P_0(A + Bc_0) - \lambda_c P_0 \leq 0,$$
(19)

$$P_{s}(\beta_{2}c_{1} + (L + MJ)A(L + MJ)^{-1}) + (\beta_{2}c_{1}) + (\beta_{$$

$$+(L+MJ)A(L+MJ)^{-1}P_s + \lambda_c P_s \leq 0, \qquad (20)$$

$$P_{s}(A + Bc_{2}) + (A + Bc_{2})^{T}P_{s} + \lambda_{c}P_{s} \leq 0.$$
(21)

If either of the following cases holds, then the trajectory x_d is asymptotically stable with respect to *d*.

(1) $\lambda_c < 0, \lambda_d \leq 0$,

- (2) all trajectories of (1) have minimal average inter-jump time $2\tau > 0$, $\lambda_c \leq 0$ and $\lambda_d + \lambda_c \tau < 0$,
- (3) all trajectories of (1) have maximal average inter-jump time $2\tau > 0, \lambda_d \leq 0$ and $\lambda_d + \lambda_c \tau < 0$.

Proof. The proof is given in Appendix B.

6. Example

We now present hybrid system and design a control law for which a maximal dwell-time argument proves asymptotic stability of the reference trajectory. Consider a single degree-of-freedom system with a damper with damping constant c > 0 and a spring with stiffness k > 0 and unloaded position $x = \bar{x}_1$, as shown in Fig. 2. Impacts can only occur at the constraint at $x_1 = 0$. Let the impacts be described by a restitution coefficient $\varepsilon = 0.9$. Hence,



Fig. 2. Dissipative mechanical system.

the impacts are dissipative, which allows to study the stability of the trajectory using a maximal average inter-jump time result. Assuming that finite constraint forces can be ignored, i.e. persistent contact does not occur, the hybrid system is described by (11) with

$$A = \begin{pmatrix} 0 & 1 \\ -k & -c \end{pmatrix}, \quad B = \begin{pmatrix} 0 \\ 1 \end{pmatrix}, \quad E = \begin{pmatrix} 0 \\ k\bar{x}_1 \end{pmatrix}, \quad L = -\varepsilon I_2,$$

$$J = \begin{pmatrix} 1 & 0 \end{pmatrix}, \quad K = 0, \quad H = 0, \quad s = -1,$$

$$z_1 = \begin{pmatrix} 0 & 1 \end{pmatrix}, \quad z_2 = 0$$

and the set C is selected to exclude the origin. The parameters $\bar{x}_1 = 1, k = 1$ and c = 0.02 are used.

Let the reference trajectory x_d be a solution to (11) for a feedforward function $u = u_{\rm ff}(t) = 100 \cos(\omega t)$, with $\omega = 0.4$. This forcing is selected such that the reference trajectory x_d with initial condition $x_d(0, 0) = (50, 0)$ has a maximal average interjump time $\tau_d > 0$. In addition, $||x_d(t, j)|| > s$ for all $(t, j) \in \text{dom } x_d$, for some s > 0, i.e. x_d does not tend to the origin.

We now apply the constructive control law design proposed in Section 5 to enforce tracking of the trajectory x_d . Selecting P_0 = $\binom{k}{0}$ $\binom{0}{1}$ and $P_s = \frac{1}{\varepsilon} P_0$, we observe that the conditions of Lemma 3 are satisfied with $\lambda_d = \log(\varepsilon) < 0$. In addition, we observe that $c_0 = c_1 = c_2 = 0$ can be selected, such that (19)–(21) hold with $\lambda_c = 0$, as $P_0 A + A^T P_0 = \begin{pmatrix} 0 & 0 \\ 0 & -2c \end{pmatrix}$ and $P_s A + A^T P_s = \begin{pmatrix} 0 & 0 \\ 0 & -\frac{2c}{c} \end{pmatrix}$.

Then, (17) yields the control law:

$$u_{\rm fb}(t,y) = \begin{cases} 0, & (\bar{x}_d(t),y) \in S_0 \\ -\frac{1+\varepsilon}{\varepsilon} (k\bar{x}_1 + u_{\rm ff}(t)), & (\bar{x}_d(t),y) \in S_1 \\ -(1+\varepsilon)(k\bar{x}_1 + u_{\rm ff}(t)), & (\bar{x}_d(t),y) \in S_2. \end{cases}$$
(22)

As the trajectory x_d has a maximal average inter-jump time, denoted τ_d , nearby trajectories will have the same behaviour. Hence, selecting $v_L > 0$ sufficiently small and restricting our attention to the hybrid system (5) with flow set $C_e \cap V_L$ and jump set $D_e \cap V_L$, with $V_L = V^{-1}([0, v_L])$, we conclude that x also has a maximal average dwell-time τ_x , with τ_x close to τ_d . Hence, the trajectory of the embedded system (5) has a maximal average inter-jump time $\frac{\max(\tau_d, \tau_x)}{2} > 0$. Consequently, case (3) of Theorem 4 proves that the trajectory is (locally) asymptotically stabilised with respect to d by the control law (22).

In Fig. 3, the performance of this controller is illustrated and a trajectory with initial condition x(0, 0) = (100, 0) is shown. The achieved stability of x_d with respect to d clearly corresponds to desirable behaviour.

From the structure of the control law (22), we observe that no control is active when $V(\bar{\varphi}_y(t,j), x_d(t,j)) = \|\varphi_y(t,j) - x_d(t,j)\|_{P_0}^2$. In fact, the dissipative effect of both the damping force $c\dot{x}$ and the jump map implies that no control is needed during these time intervals. The control input *u* only needs to compensate the destabilising effect of the forcing term $E + Bu_{\rm ff}$ during the "peaks" of the Euclidean error.

7. Conclusion

In this paper, we considered the stability of time-varying and jumping trajectories of hybrid systems with state-triggered jumps. This requires the comparison of different trajectories of



Fig. 3. (a) and (b) Reference trajectory x_d and plant trajectory x for the dissipative mechanical system and periodic forcing. (c) Euclidean tracking error. (d) Distance function (2). (e) Control force u.

a hybrid system for which we proposed a novel systematic distance function design, because the standard Euclidean distance is not adequate. Sufficient conditions for stability in terms of this distance function were formulated using Lyapunov functions that can exploit maximum or minimum average inter-jump time properties and that have sub-level sets that can be partitioned in disconnected domains. In fact, when the jump map is an affine function and the jump set a hyperplane, a systematic design procedure for piecewise quadratic Lyapunov functions was proposed as well. Based on the general theory and the specific matrix conditions for the piecewise quadratic Lyapunov function design, we designed a switched tracking control law for hybrid systems that only allow control during flow. A numerical example illustrates the applicability of our results leading to a control law that achieves accurate tracking. Moreover, the example nicely shows that the presented distance function and the corresponding asymptotic stability notion do indeed correspond to desired tracking behaviour.

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Appendix A. Alternative distance function

The distance function (2) is not necessarily continuous over jumps when evaluated along solutions to (1). When *G* is a single-valued and invertible function, such a continuity property could be induced by the function:

$$d_{Q}(x, y) = \inf_{\substack{N \in \mathbb{N} \\ y^{0} = x, x^{N+1} = y}} \inf_{\substack{x^{0}, y^{i} > x \\ y^{0} = x, x^{N+1} = y}} \sum_{i=0}^{N} \|y^{i} - x^{i+1}\|$$

that coincides with the quotient metric on the quotient space generated by the equivalence $x \sim y$ if $(x, y) \in A$. This quotient space has been suggested in Lygeros, Johansson, Simić, Zhang, and Sastry (2003) to study hybrid systems. We note that when *G* is noninvertible, then $d_Q(x, y) = 0 \Leftrightarrow (x, y) \in A$ may not hold. To allow for non-invertible jump maps, we prefer the distance function *d* in (2) over d_0 .

Appendix B. Proofs

Proof of Theorem 2. We restrict our attention to maximal trajectories φ_q to (5) that represent φ_x in the first *n* states. These trajectories always exist, which follows from the comparison of (5) and (11) and the fact that φ_x is a trajectory to (1). The observation that $\overline{\varphi}_y$ is a reparameterisation of a trajectory φ_y for (1), and both φ_x and φ_y are unbounded in *t*-direction by Assumption 2, proves that the trajectory φ_q is unbounded in *t*-direction.

We first prove that $V(\varphi_q(t, j)) < v_L$ for all $(t, j) \in \text{dom } \varphi_q$ and all trajectories φ_q of (5) if $\bar{k}V(\varphi_q(t_0, 0)) < v_L$, where \bar{k} is chosen as $\bar{k} = 1$ if (1) holds, $\bar{k} = e^{\lambda_d N_0}$ if (2) holds and $\lambda_d \ge 0$, and $\bar{k} = e^{\lambda_c N_0 \tau}$ if (3) holds and $\lambda_c \ge 0$, with N_0 given in Definition 3. Observe that if all trajectories of (1) have a minimal or maximal average interjump time 2τ , then (5) has minimal or maximal average interjump time τ .

To prove that the values of \bar{k} defined above are appropriate, for the sake of contradiction, suppose that $\bar{k}V(\varphi_q(t_0, 0)) < v_L$ and there exists a time $(t_0 + \bar{T}, \bar{J}) \in \text{dom } \varphi_q$, $\bar{T}, \bar{J} \ge 0$, such that $V(\varphi_q(t_0 + \bar{T}, \bar{J})) \ge v_L$. Hence, there exist $T \le \bar{T}$ and $J \le \bar{J}$ such that $(t_0 + T, J) \in \text{dom } \varphi_q$ and

$$V(\varphi_q(t_0 + T, J)) \ge v_L, \tag{B.1}$$

but $V(\varphi_q(t,j)) < v_L$ for all $(t,j) \in R := \{(t,j) \in \text{dom } \varphi_q \mid t < t_0 + T \lor j < J\}.$

Since φ_q represents φ_x in the first *n* states, (9)–(10) imply that $V(g) \leq e^{\lambda_d} V(\varphi_q(t,j))$ and $\left(\frac{\partial V}{\partial q}\Big|_{\varphi_q(t,j)}, f\right) \leq \lambda_c V(\varphi_q(t,j))$ hold for all $(t,j) \in R, f \in \overline{F}_e(t, \varphi_q(t,j))$ and $g \in G_e(\varphi_q(t,j))$.

Analogue to Sanfelice et al. (2014), we study the function $(t,j) \mapsto w(t,j) := V(\bar{\varphi}_x(t,j), \bar{\varphi}_y(t,j))$ along the given solution φ_q over the time domain R and we introduce scalars $\{t_j\}$ such that $R = \bigcup_j ([t_j, t_{j+1}] \times \{j\})$. As, for each j, the functions $\bar{\varphi}_x, \bar{\varphi}_y$ are absolutely continuous in t in the time interval $[t_j, t_{j+1}] \times \{j\}, w(t, j)$ is absolutely continuous in t as well. Evaluating $\dot{w}(t, j) = \frac{\partial V}{\partial q} f$ for some $f \in \bar{F}_e(t, (\bar{\varphi}_x(t, j), \bar{\varphi}_y(t, j)))$, we find with (10) that $\dot{w}(t, j) \leq \lambda_c w(t, j)$. With the comparison lemma, Khalil (2002, Lemma 3.4), we find $w(t_{j+1}, j) = e^{\lambda_c (t_{j+1} - t_j)} w(t_j, j)$ for all j. For a subsequent jump, (9) yields $w(t_{j+1}, j + 1) = e^{\lambda_d} w(t_{j+1}, j)$. Applying this result repetitively, we find

$$w(t_0 + T, j) = V(\varphi_q(t_0 + T, J)) \le e^{\lambda_c T + \lambda_d J} V(\varphi_q(t_0, 0)).$$
(B.2)

If case (1) of the theorem holds, we directly observe $V(\varphi_q(t_0 + T, J)) \leq V(\varphi_q(t_0, 0))$, contradicting (B.1). If $\lambda_d \geq 0$ and case (2) holds, then the definition of minimal average inter-jump time



Fig. B.1. The three nodes indicate when *x* and *y* may jump provided $V(x, y) \le v_L$, with v_L sufficiently small. When the conditions of Lemma 3 hold and, in addition, $V(x, y) \le \max(1, e^{-\lambda d})v_L$ right before a jump, then this jump satisfies the scenarios depicted by arrows.

yields $\lambda_c T + \lambda_d J \leq \frac{T}{\tau} (\lambda_c \tau + \lambda_d) + \lambda_d N_0 \leq \lambda_d N_0$, such that with (B.2) we find $V(\varphi_q(t_0 + T, J)) \leq \bar{k}V(\varphi_q(t_0, 0)) < v_L$, contradicting (B.1). If $\lambda_c \geq 0$ and case (3) holds, then applying the definition of maximal average inter-jump time, we observe that $\lambda_c T + \lambda_d J \leq (\lambda_d + \lambda_c \tau)J + \tau N_0 \lambda_c \leq \lambda_c \tau N_0$. Substituting this inequality in (B.2) we find $V(\varphi_q(t_0 + T, J)) \leq \bar{k}V(\varphi_q(t_0, 0)) < v_L$, contradicting (B.1). A contradiction has been obtained in all three cases, proving that $\bar{k}V(\varphi_q(t_0, 0)) < v_L$ implies $\varphi_q(t, j) \in V_L$ for all $(t, j) \in \text{dom } \varphi_q$. Hence, $V(\varphi_q(t_0, 0)) \leq \frac{v_L}{k}$ implies that, for all $(t_0 + t, j) \in \text{dom } \varphi_q$, $V(\varphi_q(t_0 + t, j)) \leq e^{\lambda_c t + \lambda_d J}V(\varphi_q(t_0, 0))$.

Assumption 2 states that all trajectories of (1) are unbounded in *t*-direction, which implies $G(D) \subseteq C \cup D$. Hence, we find $\varphi_q(t_0 + t, j) \in C_e \cup D_e$ for all $(t_0 + t, j) \in \text{dom } \varphi_q$, and we can use (8). Consequently, $d(\varphi_q(t_0 + t, j)) \leq \alpha_1^{-1}(e^{\lambda_c t + \lambda_d j}\alpha_2(d(\varphi_q(t_0, 0))))$. With the inequalities for $\lambda_c t + \lambda_d j$ derived above, we conclude that in any of the three cases of the theorem, $d(\varphi_q(t_0 + t, j)) \leq \alpha_1^{-1}(\bar{k}\alpha_2(d(\varphi_q(t_0, 0))))$, proving stability with respect to *d*. Again using the mentioned inequalities, we observe that $\lambda_c t + \lambda_d j \rightarrow -\infty$ along the solutions (this limit can be used since all trajectories are unbounded in *t*-direction, cf. Assumption 2), such that $d(\varphi_q(t_0 + t, j)) \rightarrow 0$. This proves asymptotic stability.

When (9) and (10) hold for all *y* such that $(\varphi_x(t, j), y) \in C_e \cup D_e$, then the upper bounds on $d(\varphi_q(t_0 + t, j))$ prove global asymptotic stability. \Box

The proof of Lemma 3 employs Lemmas 3 and 7 in Benjamin Biemond, Heemels, Sanfelice, and van de Wouw (2014), which hinge on the observation in Biemond et al. (2014) that the set V_L can be partitioned in three separated sets S_0 , S_1 , S_2 where the minimiser of (13) is $||x - y||_{P_0}^2$, $||x - \bar{G}(y)||_{P_s}^2$ or $||\bar{G}(x) - y||_{P_s}^2$, respectively, and, in addition, the jumps of the system (5) are restricted to the scenarios in Fig. B.1. Hence, Lemma 3 is proven by checking (9) along the scenarios in Fig. B.1.

Proof of Lemma 3. To prove the lemma, first, we observe that Biemond et al. (2014, Lemma 7) directly guarantees that there exist functions α_1 , α_2 satisfying (8). In addition, Biemond et al. (2014, Lemma 3) directly proves that there exists a sufficiently small $v_L > 0$ such that *V* is smooth in an open domain containing V_L . It remains to be proven that (14)–(15) imply (9).

Jumps of (11) may trigger jumps between the sets S_0 , S_1 and S_2 . From item (2) in Biemond et al. (2014, Lemma 3), we observe that for $(x, y) \in S_1 \cap V_L$ and $(x, y) \in S_2 \cap V_L$ jumps of x and y, respectively, are not feasible. Consequently, when $(x, y) \in S_0$, both x and y can jump, while from $(x, y) \in S_1$, only a jump of y is feasible, and $(x, y) \in S_2$ implies $x \notin D$. We will now prove that (9) holds along these four jumps:

(a) We first study the jump $(x, y) \rightarrow (G(x), y)$, with $(x, y) \in S_0$. Since (3) of Biemond et al. (2014, Lemma 3) implies that $\bar{G}(y) = (L + MJ)y + H + MK$ as $z_1y + z_2 \leq 0$ and $x \in D$ implies $\bar{G}(x) = G(x) = (L + MJ)x + H + MK$, we observe

that $V(G(x), y) \leq ||G(x) - \bar{G}(y)||_{P_s}^2 = ||\bar{G}(x) - \bar{G}(y)||_{P_s}^2 = (x - y)^T (L + MJ)^T P_s (L + MJ)(x - y)$, such that (14) implies that (9) holds.

- (b) For a jump $(x, y) \rightarrow (x, G(y))$ with $(x, y) \in S_1$, we observe $V(x, G(y)) \leq ||x G(y)||_{P_0}^2 = ||x \overline{G}(y)||_{P_0}^2$, as $y \in D$. Hence, (15) implies (9) in this case.
- (c) For a jump $(x, y) \rightarrow (x, G(y))$, with $(x, y) \in S_0$, (9) directly follows from combining (a) with the symmetry relation V(x, y) = V(y, x).
- (d) For a jump $(x, y) \rightarrow (G(x), y)$ with $(x, y) \in S_2$, symmetry of V and (b) imply (9).

Hence, we have proven that (9) holds over all feasible jumps, therewith concluding the proof of the lemma. $\hfill\square$

Proof of Theorem 4. We prove this theorem by application of Theorem 2. Lemma 3 proves that (8) and (9) hold for some $v_L > 0$. Hence, we now show that the assumptions in the theorem prove that (10) is satisfied in the sub-level set $V_L = V^{-1}([0, v_L])$.

According to Lemma 3, *V* is differentiable in *V*_L, such that we evaluate $\langle \frac{\partial V}{\partial q} |_q, f \rangle$ for $f \in \overline{F}_e(t, x_d(t, j), y)$ only when $q = (x_d(t, j), y) \in V_L \cap C_e$, where, for almost all t, \overline{F}_e is single-valued, and we distinguish the three cases given by the minimisers of (13). If $(x_d(t, j), y) \in S_0 \cap V_L$, then

$$\frac{\partial V}{\partial q} = 2(x_d(t, j) - y)^T P_0 \begin{pmatrix} I_n & -I_n \end{pmatrix}$$

and

$$\bar{F}_e = \begin{pmatrix} Ax_d(t,j) + E + Bu_{\rm ff}(t) \\ Ay + E + B(u_{\rm ff}(t) - c_0(x_d(t,j) - y)) \end{pmatrix},$$

such that (10) is guaranteed by (19).

If $(x_d(t, j), y) \in S_1 \cap V_L$, then (3) of Biemond et al. (2014, Lemma 3) implies G(y) = (L + MJ)y + H + MK. Consequently

$$\frac{\partial V}{\partial q} = 2s_1^T P_s \left(I_n \quad -(L + MJ) \right)$$

and

$$\bar{F}_{e}(t, x_{d}(t, j), y) = \begin{pmatrix} Ax_{d}(t, j) + E + Bu_{\text{ff}}(t) \\ Ay + E + B(u_{\text{ff}}(t) - \frac{\beta_{2}^{T}\beta_{1}(t)}{\beta_{2}^{T}\beta_{2}} - c_{1}s_{1}) \end{pmatrix}$$

with $s_1 = x_d(t, j) - \bar{G}(y)$ holds. Hence, we obtain $\frac{\partial V}{\partial q} \bar{F}_e(t, x, y) = 2s_1^T P_s(Ax_d(t, j) + E + Bu_{\rm ff}(t)) - (L + MJ)Ay - (L + MJ)E - (L + MJ)Bu_{\rm ff(t)} - \frac{\beta_2 \beta_2^T}{\beta_2^T \beta_2} \beta_1(t) - (L + MJ)Bc_1s_1$. With (18), we find $\frac{\beta_2 \beta_2^T}{\beta_2^T \beta_2} \beta_1(t) = \beta_1(t)$, such that $\frac{\partial V}{\partial q} \bar{F}_e(t, x_d(t, j), y)$

$$= 2s_1^T P_s(Ax_d(t, j) + (I - L - MJ)(E + Bu_{\rm ff}(t))) - (L + MJ)Ay - \beta_1(t) + \beta_2 c_1 s_1).$$
(B.3)

Since $y = (L+MJ)^{-1}(-s_1 + x_d(t, j) - H - MK) = -(L+MJ)^{-1}s_1 + \bar{G}^{\circ}(x_d(t, j))$, we obtain

$$\frac{\partial V}{\partial q} \bar{F}_e(t, x_d(t, j), y) = 2s_1^T P_s((L + MJ)A(L + MJ)^{-1} + \beta_2 c_1)s_1,$$
(B.4)

where we used the design of β_1 . Hence, (20) guarantees that (10) holds in this case.

Now, we focus on the case $(x_d(t, j), y) \in S_2 \cap V_L$. In that case, from (3) of Biemond et al. (2014, Lemma 3), we observe that $\max(0, z_1y + z_2) = 0$ follows from $(x_d(t, j), y) \in S_2 \cap V_L$. Hence,

$$\frac{\partial V}{\partial q} = 2s_2^T P_s \left(L + MJ - I_n \right)$$

and

$$\bar{F}_e(t, x_d(t, j), y) = \begin{pmatrix} Ax_d(t, j) + E + Bu_{\rm ff}(t) \\ Ay + E + B\left(u_{\rm ff}(t) - \frac{\beta_4^T \beta_3(t)}{\beta_4^T \beta_4} + c_2 s_2\right) \end{pmatrix}$$

with $s_2 = \bar{G}(x_d(t,j)) - y$. From (18) follows $\frac{\beta_4 \beta_4^T}{\beta_4^T \beta_4} \beta_3(t) = \beta_3(t)$, such that $\frac{\partial V}{\partial q} \bar{F}_e(t, x_d(t,j), y) = 2s_2^T P_s (As_2 - \beta_3(t) + (L + MJ - I_n))$ $\begin{pmatrix} Ax_d(t,j) + Bul_{\text{ff}}(t) + E \\ A\bar{G}(x_d(t,j)) + Bul_{\text{ff}}(t) + E \end{pmatrix} + Bc_2s_2$, where we used $y = \bar{G}(x_d(t,j)) - s_2$. With the design of β_3 , β_4 , we find

$$\frac{\partial V}{\partial q}\overline{F}_e(t, x_d(t, j), y) = 2s_2^T P_s(A + \beta_4 c_2)s_2, \tag{B.5}$$

such that (21) proves that (10) holds in this case. Consequently, if (19)–(21) hold, (10) is obtained. Hence, Theorem 2 proves that x_d is asymptotically stable with respect to d. \Box

References

- Angeli, D. (2002). A Lyapunov approach to incremental stability properties. IEEE Transactions on Automatic Control, 47(3), 410–421.
- Aubin, J.-P., & Frankowska, H. (2009). Modern birkhäuser classics, Set-valued analysis. Boston: Birkhäuser.
- Biemond, J. J. B., Heemels, W. P. M. H., Sanfelice, R. G., & van de Wouw, N. (2015). Constructing distance functions and piecewise quadratic Lyapunov functions for stability of hybrid trajectories. In Proceedings of the 54th IEEE Conference on Decision and Control, December 15–18, 2015, Osaka, Japan.
- Biemond, J. J. B., Heemels, W. P. M. H., Sanfelice, R. G., & van de Wouw, N. (2014). Distance function design and Lyapunov techniques for the stability of hybrid trajectories. Technical report. Arxiv: https://arxiv.org/abs/1501.00161.
- Biemond, J. J. B., van de Wouw, N., Heemels, W. P. M. H., & Nijmeijer, H. (2013). Tracking control for hybrid systems with state-triggered jumps. *IEEE Transactions on Automatic Control*, 58(4), 876–890.

Brogliato, B. (1999). Nonsmooth mechanics. London: Springer-Verlag.

- Broucke, M., & Arapostathis, A. (2002). Continuous selections of trajectories of hybrid systems. Systems & Control Letters, 47, 149–157.
- Filippov, A. F. (1988). Mathematics and its applications (soviet series): vol. 18. Differential equations with discontinuous righthand sides. Dordrecht: Kluwer Academic Publishers.
- Forni, F., Teel, A. R., & Zaccarian, L. (2013). Follow the bouncing ball: global results on tracking and state estimation with impacts. *IEEE Transactions on Automatic Control*, 58(6), 1470–1485.
- Galeani, S., Menini, L., Potini, A., & Tornambè, A. (2008). Trajectory tracking for a particle in elliptical billiards. *International Journal of Control*, 81(2), 189–213.
- Goebel, R., Sanfelice, R. G., & Teel, A. R. (2012). Hybrid dynamical systems: Modeling, stability and robustness. Princeton: Princeton University Press.
- Heemels, W. P. M. H., de Schutter, B., Lunze, J., & Lazar, M. (2010). Stability analysis and controller synthesis for hybrid dynamical systems. *Philosophical Transactions of the Royal Society of London, Series A, Mathematical, Physical and Engineering Sciences*, 368(1930), 4937–4960.
- Hespanha, J. P., Liberzon, D., & Teel, A. R. (2008). Lyapunov conditions for input-tostate stability of impulsive systems. *Automatica*, 44(11), 2735–2744.
- Khalil, H. K. (2002). Nonlinear systems (3rd ed.). Upper Saddle River: Prentice Hall.
- Leine, R. I., & van de Wouw, N. (2008). Lecture notes in applied and computational mechanics: vol. 36. Stability and convergence of mechanical systems with unilateral constraints. Berlin: Springer-Verlag.
- Li, Y., Phillips, S., & Sanfelice, R. G. (2016). Basic properties and characterizations of incremental stability prioritizing flow time for a class of hybrid systems. *Systems & Control Letters*, 90, 7–15.
- Lygeros, J., Johansson, K. H., Simić, S. N., Zhang, Jun, & Sastry, S. S. (2003). Dynamical properties of hybrid automata. *IEEE Transactions on Automatic Control*, 48(1), 2–17.
- Menini, L., & Tornambè, A. (2001). Asymptotic tracking of periodic trajectories for a simple mechanical system subject to nonsmooth impacts. *IEEE Transactions on Automatic Control*, 46(7), 1122–1126.
- Morărescu, I. C., & Brogliato, B. (2010). Trajectory tracking control of multiconstraint complementarity Lagrangian systems. *IEEE Transactions on Automatic Control*, 55(6), 1300–1313.
- Postoyan, R., Tabuada, P., Nesic, D., & Anta, A. (2015). A framework for the eventtriggered stabilization of nonlinear systems. *IEEE Transactions on Automatic Control*, 60(4), 982–996.
- Rüffer, B. S., van de Wouw, N., & Mueller, M. (2013). Convergent systems vs. incremental stability. Systems & Control Letters, 62(3), 277–285.
- Sanfelice, R. G., Biemond, J. J. B., van de Wouw, N., & Heemels, W. P. M. H. (2014). An embedding approach for the design of state-feedback tracking controllers for references with jumps. *International Journal of Robust and Nonlinear Control*, 24(11), 1585–1608.

Schatzman, M. (1998). Uniqueness and continuous dependence on data for onedimensional impact problems. *Mathematical and Computer Modelling*, 28(4–8), 1, 192

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