

Backstepping controller synthesis and characterizations of incremental stability[☆]



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ABSTRACT

Incremental stability is a property of dynamical and control systems, requiring the uniform asymptotic stability of every trajectory, rather than that of an equilibrium point or a particular time-varying trajectory. Similarly to stability, Lyapunov functions and contraction metrics play important roles in the study of incremental stability. In this paper, we provide characterizations and descriptions of incremental stability in terms of existence of coordinate-invariant notions of incremental Lyapunov functions and contraction metrics, respectively. Most design techniques providing controllers rendering control systems incrementally stable have two main drawbacks: they can only be applied to control systems in either parametric-strict-feedback or strict-feedback form, and they require these control systems to be smooth. In this paper, we propose a design technique that is applicable to larger classes of control systems, including a class of non-smooth control systems. Moreover, we propose a recursive way of constructing contraction metrics (for smooth control systems) and incremental Lyapunov functions which have been identified as a key tool enabling the construction of finite abstractions of nonlinear control systems, the approximation of stochastic hybrid systems, source-code model checking for nonlinear dynamical systems and so on. The effectiveness of the proposed results in this paper is illustrated by synthesizing controllers rendering two non-smooth control systems incrementally stable. The first example aims to show how to recursively construct the incremental Lyapunov functions. The second example aims to show the key role of the computed incremental Lyapunov function in constructing a finite abstraction that is equivalent to the system under study.

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1. Introduction

Incremental stability is a stronger property than stability for dynamical and control systems. In incremental stability, focus is on convergence of trajectories with respect to each other rather than with respect to an equilibrium point or a specific trajectory. Similarly to stability, Lyapunov functions play an important role in the study of incremental stability. In [1], Angeli proposed the notions of incremental Lyapunov function and incremental input-to-state Lyapunov function, and used these notions to provide characterizations of incremental global asymptotic stability (δ -GAS) and

incremental input-to-state stability (δ -ISS). Notions of δ -GAS, δ -ISS and incremental Lyapunov functions, proposed in [1], are not coordinate invariant, in general. Since most of the controller design approaches benefit from changes of coordinates, in [2], the authors proposed different notions of δ -GAS and δ -ISS which are coordinate invariant. In [3], the authors proposed notions of incremental Lyapunov function and incremental input-to-state Lyapunov function that are coordinate invariant as well. We use these new notions of Lyapunov functions to fully characterize the notions of incremental (input-to-state) stability as proposed in [2]. Furthermore, we provide sufficient conditions for coordinate invariant incremental (input-to-state) stability in the form of contraction metrics inspired by the work in [4].

The number of applications of incremental stability has increased progressively in the past years. Examples include building explicit bounds on the region of attraction in phase-locking in the Kuramoto system [5], modeling of nonlinear analog circuits [6], robustness analysis of systems over finite alphabets [7], global synchronization in networks of cyclic feedback systems [8], control reconfiguration of piecewise affine systems with actuator and

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sensor faults [9], construction of symbolic models for nonlinear control systems [10–12], and synchronization [13,14]. Unfortunately, there are very few results available in the literature regarding the design of controllers enforcing incremental stability of the resulting closed-loop systems. Therefore, there is a growing need to develop design methods rendering control systems incrementally stable.

Related works include the controller designs for convergence of Lur'e-type systems [15,16] and a class of piecewise affine systems [17] through the solution of linear matrix inequalities (LMIs). In contrast, the current paper does not require the solution of LMIs and the existence of controllers is always guaranteed for the class of systems under consideration. The quest for backstepping design approaches for incremental stability has received increasing attention recently. Recently obtained results include backstepping design approaches rendering parametric-strict-feedback¹ form systems incrementally globally asymptotically stable² using the notion of contraction metrics in [19–21], and backstepping design approaches rendering strict-feedback¹ form systems incrementally input-to-state stable³ using the notion of contraction metrics and incremental Lyapunov functions in [2,3], respectively. The results in [15] offer a backstepping design approach rendering a larger class of control systems than those in strict-feedback form input-to-state convergent, rather than incrementally input-to-state stable. We will build upon these results in [15] and extend those in the scope of incremental stability. The notion of (input-to-state) convergence requires existence of a trajectory which is bounded on the whole time axis which is not required in the case of incremental input-to-state stability. The notion of input-to-state convergence cannot be applied to the results in [10–12], which require the uniform global asymptotic stability of every trajectory rather than that of a particular trajectory that is bounded on the entire time axis. See [2,22,23], for a brief comparison between the notions of convergent system and incremental stability.

Our controller synthesis techniques improve upon most of the existing backstepping techniques in three directions:

- (1) by providing controllers enforcing not only incremental global asymptotic stability but also incremental input-to-state stability;
- (2) by being applicable to larger classes of control systems including a class of non-smooth control systems;
- (3) by providing a recursive way of constructing not only contraction metrics but also incremental Lyapunov functions.

In the first direction, our technique extends the results in [19–21], where only controllers enforcing incremental global asymptotic stability are designed. In the second direction, our technique improves the results in [19–21], which are only applicable to smooth parametric-strict-feedback form systems, and the results in [2,3], which are only applicable to smooth strict-feedback form systems. In the third direction, our technique extends the results in [19–21,2], where the authors only provide a recursive way of constructing contraction metrics, and the results in [15], where the authors do not provide a way to construct Lyapunov functions characterizing the input-to-state convergence property induced by the controller. Note that, the explicit availability of incremental Lyapunov functions is necessary in many applications. Examples include the construction of symbolic models for nonlinear control systems [11,24,25], robust test generation of hybrid systems [26],

the approximation of stochastic hybrid systems [27], and source-code model checking for nonlinear dynamical systems [28]. Note that incremental Lyapunov functions can be used as bisimulation functions, recognized as a key tool for the analysis in [26–28].

Our technical results are illustrated by designing incrementally input-to-state stabilizing controllers for two unstable non-smooth control systems that do not satisfy the assumptions required in [19–21,2,3]. The main objective of the first example is to show how the incremental Lyapunov functions can be constructed recursively using the results in this paper. Regarding the second example, we construct a finite bisimilar abstraction for the resulting incrementally stable closed-loop system using the results in [11], which, as we care to stress, only apply to incrementally stable systems with explicitly available incremental Lyapunov functions (where the latter can be constructed on the basis of the results in this paper). When a finite abstraction is available, the synthesis of the controllers satisfying logic specifications expressed in linear temporal logic or automata on infinite strings can be easily reduced to a fixed-point computation over the finite-state abstraction [29]. Note that, satisfying those specifications is difficult or impossible to enforce with conventional control design methods. Furthermore, to add a discrete component to the problem, we assume that the system is subject to a constraint expressed by a finite automaton. We synthesize another controller on top of the resulting incrementally stable closed-loop system satisfying some logic specification explained in details in the example section.

The outline of the paper is as follows. Section 2 provides some mathematical preliminaries, the definition of the class of control systems that we consider in this paper, and stability notions. Section 3 provides characterizations of incremental stability in terms of existence of incremental Lyapunov functions and contraction metrics. In Section 4, we present the proposed backstepping design approach. Two illustrative (non-smooth) examples are discussed in detail in Section 5. Finally, Section 6 concludes the paper.

2. Control systems and stability notions

2.1. Notation

The symbols \mathbb{Z} , \mathbb{N} , \mathbb{N}_0 , \mathbb{R} , \mathbb{R}^+ and \mathbb{R}_0^+ denote the set of integer, positive integer, nonnegative integer, real, positive, and nonnegative real numbers, respectively. The symbols I_m , $0_{m \times n}$, and 0_m denote the identity and zero matrices in $\mathbb{R}^{m \times m}$ and $\mathbb{R}^{m \times n}$, and the zero vector in \mathbb{R}^m , respectively. Given a vector $x \in \mathbb{R}^n$, we denote by x_i the i -th element of x , by $|x_i|$ the absolute value of x_i , and by $\|x\|$ the Euclidean norm of x ; we recall that $\|x\| = \sqrt{x_1^2 + x_2^2 + \dots + x_n^2}$ for $x \in \mathbb{R}^n$. Given a measurable function $f : \mathbb{R}_0^+ \rightarrow \mathbb{R}^n$, the (essential) supremum of f is denoted by $\|f\|_\infty$; we recall that $\|f\|_\infty := (\text{ess})\sup\{\|f(t)\|, t \geq 0\}$ and $\|f\|_{[0, \tau)} := (\text{ess})\sup\{\|f(t)\|, t \in [0, \tau)\}$. A function f is essentially bounded if $\|f\|_\infty < \infty$. For a given time $\tau \in \mathbb{R}^+$, define f_τ so that $f_\tau(t) = f(t)$, for any $t \in [0, \tau)$, and $f_\tau(t) = 0$ elsewhere; f is said to be locally essentially bounded if for any $\tau \in \mathbb{R}^+$, f_τ is essentially bounded. A function $f : \mathbb{R}^n \rightarrow \mathbb{R}_0^+$ is called radially unbounded if $f(x) \rightarrow \infty$ as $\|x\| \rightarrow \infty$. The closed ball centered at $x \in \mathbb{R}^m$ with radius ε is defined by $\mathcal{B}_\varepsilon(x) = \{y \in \mathbb{R}^m \mid \|x - y\| \leq \varepsilon\}$. A continuous function $\gamma : \mathbb{R}_0^+ \rightarrow \mathbb{R}_0^+$, is said to belong to class \mathcal{K} if it is strictly increasing and $\gamma(0) = 0$; γ is said to belong to class \mathcal{K}_∞ if $\gamma \in \mathcal{K}$ and $\gamma(r) \rightarrow \infty$ as $r \rightarrow \infty$. A continuous function $\beta : \mathbb{R}_0^+ \times \mathbb{R}_0^+ \rightarrow \mathbb{R}_0^+$ is said to belong to class \mathcal{KL} if, for each fixed s , the map $\beta(r, s)$ belongs to class \mathcal{K}_∞ with respect to r and, for each fixed nonzero r , the map $\beta(r, s)$ is decreasing with respect to s and $\beta(r, s) \rightarrow 0$ as $s \rightarrow \infty$. If $\phi : \mathbb{R}^n \rightarrow \mathbb{R}^n$ is a global diffeomorphism and $G : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$ is a smooth map, the notation $\phi^*G : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$ denotes the smooth map $(\phi^*G)(x) = (\frac{\partial \phi}{\partial x})^T G(\phi(x)) (\frac{\partial \phi}{\partial x})$. A Riemannian metric

¹ See [18] for a definition.

² Understood in the sense of Definition 2.2.

³ Understood in the sense of Definition 2.3.

$G : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$ is a smooth map on \mathbb{R}^n such that, for any $x \in \mathbb{R}^n$, $G(x)$ is a symmetric positive definite matrix [30]. For any $x \in \mathbb{R}^n$ and smooth functions $I, J : \mathbb{R}^n \rightarrow \mathbb{R}$, one can define the scalar function $\langle I, J \rangle_G$ as $I^T(x)G(x)J(x)$. We will still use the notation $\langle I, J \rangle_G$ to denote $I^T G J$ even if G does not represent a Riemannian metric. A function $\mathbf{d} : \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}_0^+$ is a metric on \mathbb{R}^n if for any $x, y, z \in \mathbb{R}^n$, the following three conditions are satisfied: (i) $\mathbf{d}(x, y) = 0$ if and only if $x = y$; (ii) $\mathbf{d}(x, y) = \mathbf{d}(y, x)$; and (iii) (triangle inequality) $\mathbf{d}(x, z) \leq \mathbf{d}(x, y) + \mathbf{d}(y, z)$. We use the pair $(\mathbb{R}^n, \mathbf{d})$ to denote a metric space \mathbb{R}^n equipped with the metric \mathbf{d} . We use the notation \mathbf{d}_G to denote the Riemannian distance function provided by the Riemannian metric G , as defined for example in [30]. We refer to the proof of Lemma 3.12 in the paper for the definition of \mathbf{d}_G . For a set $\mathcal{A} \subseteq \mathbb{R}^n$, a metric \mathbf{d} , and any $x \in \mathbb{R}^n$, we abuse the notation by using $\mathbf{d}(x, \mathcal{A})$ to denote the point-to-set distance, defined by $\mathbf{d}(x, \mathcal{A}) = \inf_{y \in \mathcal{A}} \mathbf{d}(x, y)$. A function f is said to be smooth if it is an infinitely differentiable function of its arguments. Given measurable functions $f : \mathbb{R}_0^+ \rightarrow \mathbb{R}^n$ and $g : \mathbb{R}_0^+ \rightarrow \mathbb{R}^n$, we define $\mathbf{d}(f, g)_\infty := (\text{ess})\sup\{\mathbf{d}(f(t), g(t)), t \geq 0\}$ and $\mathbf{d}(f, g)_{[0, \tau]} := (\text{ess})\sup\{\mathbf{d}(f(t), g(t)), t \in [0, \tau]\}$. The diagonal set $\Delta \subset \mathbb{R}^{2n}$ is defined as: $\Delta = \{z \in \mathbb{R}^{2n} \mid \exists x \in \mathbb{R}^n : z = [x^T, x^T]^T\}$.

2.2. Control systems

The class of control systems that we consider in this paper is formalized in the following definition.

Definition 2.1. A control system is a quadruple:

$$\Sigma = (\mathbb{R}^n, \mathcal{U}, \mathcal{f}),$$

where:

- \mathbb{R}^n is the state space;
- $\mathcal{U} \subseteq \mathbb{R}^m$ is the input set;
- \mathcal{U} is the set of all measurable, locally essentially bounded functions of time from intervals of the form $]a, b[\subseteq \mathbb{R}$ to \mathcal{U} with $a < 0$ and $b > 0$;
- $f : \mathbb{R}^n \times \mathcal{U} \rightarrow \mathbb{R}^n$ is a continuous map satisfying the following Lipschitz assumption: for every compact set $Q \subset \mathbb{R}^n$, there exists a constant $Z \in \mathbb{R}^+$ such that $\|f(x, u) - f(y, u)\| \leq Z\|x - y\|$ for all $x, y \in Q$ and all $u \in \mathcal{U}$.

A curve $\xi :]a, b[\rightarrow \mathbb{R}^n$ is said to be a *trajectory* of Σ if there exists $v \in \mathcal{U}$ satisfying:

$$\dot{\xi}(t) = f(\xi(t), v(t)),$$

for almost all $t \in]a, b[$. Although we have defined trajectories over open domains, we shall refer to trajectories $\xi : [0, t] \rightarrow \mathbb{R}^n$ defined on closed domains $[0, t]$, $t \in \mathbb{R}^+$ with the understanding of the existence of a trajectory $\xi' :]a, b[\rightarrow \mathbb{R}^n$ such that $\xi = \xi'|_{[0, t]}$ with $a < 0$ and $b > t$. We also write $\xi_{xv}(t)$ to denote the point reached at time t under the input v from initial condition $x = \xi_{xv}(0)$; the point $\xi_{xv}(t)$ is uniquely determined, since the assumptions on f ensure the existence and uniqueness of trajectories [31].

A control system Σ is said to be forward complete if every trajectory is defined on an interval of the form $]a, \infty[$. Sufficient and necessary conditions for a system to be forward complete can be found in [32]. A control system Σ is said to be smooth if f is smooth.

2.3. Stability notions

Here, we recall the notions of incremental global asymptotic stability (δ_3 -GAS) and incremental input-to-state stability (δ_3 -ISS), presented in [2].

Definition 2.2 ([2]). A control system $\Sigma = (\mathbb{R}^n, \mathcal{U}, \mathcal{f})$ is incrementally globally asymptotically stable (δ_3 -GAS) if it is forward

complete and there exist a metric \mathbf{d} and a \mathcal{KL} function β such that for any $t \in \mathbb{R}_0^+$, any $x, x' \in \mathbb{R}^n$ and any $v \in \mathcal{U}$ the following condition is satisfied:

$$\mathbf{d}(\xi_{xv}(t), \xi_{x'v}(t)) \leq \beta(\mathbf{d}(x, x'), t). \quad (2.1)$$

As defined in [1], δ -GAS requires the metric \mathbf{d} to be the Euclidean metric. However, Definition 2.2 only requires the existence of a metric. We note that while δ -GAS is not generally invariant under changes of coordinates, δ_3 -GAS is. When the origin is an equilibrium point for Σ , with $v(t) = 0$ for all $t \in \mathbb{R}_0^+$, and the map $\psi : \mathbb{R}^n \rightarrow \mathbb{R}_0^+$, defined by $\psi(\cdot) = \mathbf{d}(\cdot, 0)$, is continuous⁴ and radially unbounded, both δ_3 -GAS and δ -GAS imply global asymptotic stability.

Definition 2.3 ([2]). A control system $\Sigma = (\mathbb{R}^n, \mathcal{U}, \mathcal{f})$ is incrementally input-to-state stable (δ_3 -ISS) if it is forward complete and there exist a metric \mathbf{d} , a \mathcal{KL} function β , and a \mathcal{K}_∞ function γ such that for any $t \in \mathbb{R}_0^+$, any $x, x' \in \mathbb{R}^n$, and any $v, v' \in \mathcal{U}$ the following condition is satisfied:

$$\mathbf{d}(\xi_{xv}(t), \xi_{x'v'}(t)) \leq \beta(\mathbf{d}(x, x'), t) + \gamma(\|v - v'\|_\infty). \quad (2.2)$$

By observing (2.1) and (2.2), it is readily seen that δ_3 -ISS implies δ_3 -GAS while the converse is not true in general. Moreover, whenever the metric \mathbf{d} is the Euclidean metric, δ_3 -ISS becomes δ -ISS as defined in [1]. We note that while δ -ISS is not generally invariant under changes of coordinates, δ_3 -ISS is. When the origin is an equilibrium point for Σ , with $v(t) = 0$ for all $t \in \mathbb{R}_0^+$, and the map $\psi : \mathbb{R}^n \rightarrow \mathbb{R}_0^+$, defined by $\psi(\cdot) = \mathbf{d}(\cdot, 0)$, is continuous⁴ and radially unbounded, both δ_3 -ISS and δ -ISS imply input-to-state stability [33].

3. Characterizations of incremental stability

This section contains characterizations and descriptions of δ_3 -GAS and δ_3 -ISS in terms of existence of incremental Lyapunov functions and contraction metrics, respectively. We note that only the sufficiency part of Lyapunov characterizations of δ_3 -GAS and δ_3 -ISS were presented in [3]. In Section 4, we will use such incremental Lyapunov functions and contraction metrics to synthesize controllers rendering closed-loop systems incrementally stable.

3.1. Incremental Lyapunov function characterizations

We start by recalling the notions of an incremental global asymptotic stability (δ_3 -GAS) Lyapunov function and an incremental input-to-state stability (δ_3 -ISS) Lyapunov function, presented in [3].

Definition 3.1 ([3]). Consider a control system $\Sigma = (\mathbb{R}^n, \mathcal{U}, \mathcal{f})$ and a smooth function $V : \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}_0^+$. Function V is called a δ_3 -GAS Lyapunov function for Σ , if there exist a metric \mathbf{d} , \mathcal{K}_∞ functions $\underline{\alpha}, \bar{\alpha}$, and $\kappa \in \mathbb{R}^+$ such that:

- (i) for any $x, x' \in \mathbb{R}^n$,
 $\underline{\alpha}(\mathbf{d}(x, x')) \leq V(x, x') \leq \bar{\alpha}(\mathbf{d}(x, x'))$;
- (ii) for any $x, x' \in \mathbb{R}^n$ and any $u \in \mathcal{U}$,
 $\frac{\partial V}{\partial x} f(x, u) + \frac{\partial V}{\partial x'} f(x', u) \leq -\kappa V(x, x')$.

Function V is called a δ_3 -ISS Lyapunov function for Σ , if there exist a metric \mathbf{d} , \mathcal{K}_∞ functions $\underline{\alpha}, \bar{\alpha}, \sigma$, and $\kappa \in \mathbb{R}^+$ satisfying conditions (i) and:

- (iii) for any $x, x' \in \mathbb{R}^n$ and for any $u, u' \in \mathcal{U}$,
 $\frac{\partial V}{\partial x} f(x, u) + \frac{\partial V}{\partial x'} f(x', u') \leq -\kappa V(x, x') + \sigma(\|u - u'\|)$.

⁴ Here, continuity is understood with respect to the Euclidean metric.

To provide characterizations of δ_3 -ISS (resp. δ_3 -GAS) in terms of the existence of δ_3 -ISS (resp. δ_3 -GAS) Lyapunov functions, we need the following technical results.

Here, we introduce the following definition which was inspired by the notion of uniform global asymptotic stability (UGAS) with respect to sets, presented in [34].

Definition 3.2. A control system $\Sigma = (\mathbb{R}^n, \mathcal{U}, \mathcal{U}, f)$ is uniformly globally asymptotically stable (U_3 GAS) with respect to a set $\mathcal{A} \subseteq \mathbb{R}^n$ if it is forward complete and there exist a metric \mathbf{d} , and a \mathcal{KL} function β such that for any $t \in \mathbb{R}_0^+$, any $x \in \mathbb{R}^n$ and any $v \in \mathcal{U}$, the following condition is satisfied:

$$\mathbf{d}(\xi_{xv}(t), \mathcal{A}) \leq \beta(\mathbf{d}(x, \mathcal{A}), t). \quad (3.1)$$

We now introduce the following definition which was inspired by the notion of uniform global asymptotic stability (UGAS) Lyapunov functions in [34].

Definition 3.3. Consider a control system $\Sigma = (\mathbb{R}^n, \mathcal{U}, \mathcal{U}, f)$, a set $\mathcal{A} \subseteq \mathbb{R}^n$, and a smooth function $V : \mathbb{R}^n \rightarrow \mathbb{R}_0^+$. Function V is called a U_3 GAS Lyapunov function, with respect to \mathcal{A} , for Σ , if there exist a metric \mathbf{d} , \mathcal{K}_∞ functions $\underline{\alpha}$, $\bar{\alpha}$, and $\kappa \in \mathbb{R}^+$ such that:

- (i) for any $x \in \mathbb{R}^n$,
 $\underline{\alpha}(\mathbf{d}(x, \mathcal{A})) \leq V(x) \leq \bar{\alpha}(\mathbf{d}(x, \mathcal{A}));$
- (ii) for any $x \in \mathbb{R}^n$ and any $u \in \mathcal{U}$,
 $\frac{\partial V}{\partial x} f(x, u) \leq -\kappa V(x).$

The following theorem characterizes U_3 GAS in terms of the existence of a U_3 GAS Lyapunov function.

Theorem 3.4. Consider a control system $\Sigma = (\mathbb{R}^n, \mathcal{U}, \mathcal{U}, f)$ and a set $\mathcal{A} \subseteq \mathbb{R}^n$. If \mathcal{U} is compact and \mathbf{d} is a metric such that the function $\psi(\cdot) = \mathbf{d}(\cdot, y)$ is continuous⁴ for any $y \in \mathbb{R}^n$ then the following statements are equivalent:

- (1) Σ is forward complete and there exists a U_3 GAS Lyapunov function with respect to \mathcal{A} , equipped with the metric \mathbf{d} .
- (2) Σ is U_3 GAS with respect to \mathcal{A} , equipped with the metric \mathbf{d} .

Proof. First we show that the function $\phi(\cdot) = \mathbf{d}(\cdot, \mathcal{A})$ is a continuous function with respect to the Euclidean metric. Assume that $\{x_n\}_{n=1}^\infty$ is a converging sequence in \mathbb{R}^n with respect to the Euclidean metric, implying that $\|x_n - x^*\| \rightarrow 0$ as $n \rightarrow \infty$ for some $x^* \in \mathbb{R}^n$. By the triangle inequality, we have:

$$\mathbf{d}(x^*, y) \leq \mathbf{d}(x^*, x_n) + \mathbf{d}(y, x_n), \quad (3.2)$$

for any $n \in \mathbb{N}$ and any $y \in \mathcal{A}$. Using inequality (3.2), we obtain:

$$\begin{aligned} \phi(x^*) &= \mathbf{d}(x^*, \mathcal{A}) = \inf_{y \in \mathcal{A}} \mathbf{d}(x^*, y) \\ &\leq \inf_{y \in \mathcal{A}} \{\mathbf{d}(x^*, x_n) + \mathbf{d}(y, x_n)\} \\ &= \mathbf{d}(x^*, x_n) + \inf_{y \in \mathcal{A}} \mathbf{d}(y, x_n) = \mathbf{d}(x^*, x_n) + \phi(x_n), \end{aligned} \quad (3.3)$$

for any $n \in \mathbb{N}$. Using inequality (3.3) and the continuity assumption on \mathbf{d} , implying that $\lim_{n \rightarrow \infty} \mathbf{d}(x^*, x_n) = \mathbf{d}(x^*, x^*) = 0$, we obtain for any $n \in \mathbb{N}$:

$$\begin{aligned} \phi(x^*) &\leq \inf_{m \geq n} \{\mathbf{d}(x^*, x_m) + \phi(x_m)\} \\ &\Rightarrow \phi(x^*) \leq \liminf_{n \rightarrow \infty} \phi(x_n), \end{aligned} \quad (3.4)$$

where a limit inferior exists because a lower bounded sequence of real numbers always admit a greatest lower bound [35]. By doing the same analysis, we have:

$$\phi(x^*) \geq \limsup_{n \rightarrow \infty} \phi(x_n), \quad (3.5)$$

where a limit superior exists because an upper bounded sequence of real numbers always admit a lowest upper bound [35]. Using inequalities (3.4) and (3.5), one obtains:

$$\phi(x^*) = \lim_{n \rightarrow \infty} \phi(x_n),$$

implying that ϕ is a continuous function with respect to the Euclidean metric. Since $\phi(\cdot) = \mathbf{d}(\cdot, \mathcal{A})$ is a continuous, positive semi-definite function, by choosing $\omega_1(\cdot) = \omega_2(\cdot) = \mathbf{d}(\cdot, \mathcal{A})$ in Theorem 1 in [36], the proof completes.

Before showing the main results, we need the following technical lemma, inspired by Lemma 2.3 in [1].

Lemma 3.5. Consider a control system $\Sigma = (\mathbb{R}^n, \mathcal{U}, \mathcal{U}, f)$. If Σ is δ_3 -GAS, then the control system $\hat{\Sigma} = (\mathbb{R}^{2n}, \mathcal{U}, \mathcal{U}, \hat{f})$, where $\hat{f}(\zeta, v) = [f(\xi_1, v)^T, f(\xi_2, v)^T]^T$, and $\zeta = [\xi_1^T, \xi_2^T]^T$, is U_3 GAS with respect to the diagonal set Δ .

Proof. Since Σ is δ_3 -GAS, there exists a metric $\mathbf{d} : \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}_0^+$ such that property (2.1) is satisfied. Now we define a new metric $\hat{\mathbf{d}} : \mathbb{R}^{2n} \times \mathbb{R}^{2n} \rightarrow \mathbb{R}_0^+$ by:

$$\hat{\mathbf{d}}(z, z') = \mathbf{d}(x_1, x'_1) + \mathbf{d}(x_2, x'_2), \quad (3.6)$$

for any $z = [x_1^T, x_2^T]^T, z' = [x'_1{}^T, x'_2{}^T]^T \in \mathbb{R}^{2n}$. It can be readily checked that $\hat{\mathbf{d}}$ satisfies all three conditions of a metric. Now we show that $\hat{\mathbf{d}}(z, \Delta)$, for any $z = [x_1^T, x_2^T]^T \in \mathbb{R}^{2n}$, is proportional to $\mathbf{d}(x_1, x_2)$ that will be exploited later in the proof. We have:

$$\begin{aligned} \hat{\mathbf{d}}(z, \Delta) &= \inf_{z' \in \Delta} \hat{\mathbf{d}}(z, z') = \inf_{x' \in \mathbb{R}^n} \hat{\mathbf{d}}\left(\begin{bmatrix} x_1 \\ x_2 \end{bmatrix}, \begin{bmatrix} x' \\ x' \end{bmatrix}\right) \\ &= \inf_{x' \in \mathbb{R}^n} \{\mathbf{d}(x_1, x') + \mathbf{d}(x_2, x')\} \\ &\leq \inf_{x' = x_1} \{\mathbf{d}(x_1, x') + \mathbf{d}(x_2, x')\} \\ &= \mathbf{d}(x_1, x_1) + \mathbf{d}(x_1, x_2) = \mathbf{d}(x_1, x_2). \end{aligned} \quad (3.7)$$

Since \mathbf{d} is a metric, by using the triangle inequality, we have: $\mathbf{d}(x_1, x_2) \leq \mathbf{d}(x_1, x') + \mathbf{d}(x_2, x')$ for any $x' \in \mathbb{R}^n$, implying that:

$$\mathbf{d}(x_1, x_2) \leq \inf_{x' \in \mathbb{R}^n} \{\mathbf{d}(x_1, x') + \mathbf{d}(x_2, x')\} = \hat{\mathbf{d}}(z, \Delta). \quad (3.8)$$

Hence, using (3.7) and (3.8), one obtains:

$$\mathbf{d}(x_1, x_2) \leq \hat{\mathbf{d}}(z, \Delta) \leq \mathbf{d}(x_1, x_2) \Rightarrow \mathbf{d}(x_1, x_2) = \hat{\mathbf{d}}(z, \Delta). \quad (3.9)$$

Using equality (3.9) and property (2.1), we have:

$$\begin{aligned} \hat{\mathbf{d}}(\zeta_{zv}(t), \Delta) &= \hat{\mathbf{d}}\left(\begin{bmatrix} \xi_{x_1 v}(t) \\ \xi_{x_2 v}(t) \end{bmatrix}, \Delta\right) = \mathbf{d}(\xi_{x_1 v}(t), \xi_{x_2 v}(t)) \\ &\leq \beta(\mathbf{d}(x_1, x_2), t) = \beta(\hat{\mathbf{d}}(z, \Delta), t), \end{aligned}$$

for any $t \in \mathbb{R}_0^+$, any $z = [x_1^T, x_2^T]^T \in \mathbb{R}^{2n}$ and any $v \in \mathcal{U}$, where $\zeta_{zv} = [\xi_{x_1 v}^T, \xi_{x_2 v}^T]^T$. Hence, $\hat{\Sigma}$ is U_3 GAS with respect to Δ .

We can now provide the characterization of δ_3 -GAS in terms of existence of a δ_3 -GAS Lyapunov function.

Theorem 3.6. Consider a control system $\Sigma = (\mathbb{R}^n, \mathcal{U}, \mathcal{U}, f)$. If \mathcal{U} is compact and \mathbf{d} is a metric such that the function $\psi(\cdot) = \mathbf{d}(\cdot, y)$ is continuous⁴ for any $y \in \mathbb{R}^n$ then the following statements are equivalent:

- (1) Σ is forward complete and there exists a δ_3 -GAS Lyapunov function, equipped with the metric \mathbf{d} .
- (2) Σ is δ_3 -GAS, equipped with the metric \mathbf{d} .

Proof. The proof from (1) to (2) has been provided in Theorem 2.6 in [3], even in the absence of the compactness and continuity assumptions on U and \mathbf{d} , respectively. We now prove that (2) implies (1). Since Σ is δ_3 -GAS, using Lemma 3.5, we conclude that the control system $\widehat{\Sigma}$, defined in Lemma 3.5, is U_3 GAS with respect to the diagonal set Δ . Since $\psi(\cdot) = \mathbf{d}(\cdot, y)$ is continuous⁴ for any $y \in \mathbb{R}^n$, it can be easily verified that the function $\widehat{\psi}(\cdot) = \widehat{\mathbf{d}}(\cdot, z')$ is also continuous⁴ for any $z' \in \mathbb{R}^{2n}$, where the metric $\widehat{\mathbf{d}}$ was defined in Lemma 3.5. Using Theorem 3.4, we conclude that there exists a U_3 GAS Lyapunov function $V : \mathbb{R}^{2n} \rightarrow \mathbb{R}_0^+$, with respect to the diagonal set Δ , for $\widehat{\Sigma}$. Thanks to the special form of $\widehat{\Sigma}$, using the equality (3.9), and slightly abusing notation, the function V satisfies:

$$\begin{aligned} \text{(i)} \quad & \underline{\alpha} \left(\widehat{\mathbf{d}} \left(\begin{bmatrix} x \\ x' \end{bmatrix}, \Delta \right) \right) \leq V \left(\begin{bmatrix} x \\ x' \end{bmatrix} \right) \leq \overline{\alpha} \left(\widehat{\mathbf{d}} \left(\begin{bmatrix} x \\ x' \end{bmatrix}, \Delta \right) \right) \Rightarrow \underline{\alpha}(\mathbf{d}(x, x')) \leq V(x, x') \leq \overline{\alpha}(\mathbf{d}(x, x')); \\ \text{(ii)} \quad & \left[\frac{\partial V}{\partial x} \frac{\partial V}{\partial x'} \right] \begin{bmatrix} f(x, u) \\ f(x', u) \end{bmatrix} \leq -\kappa V \left(\begin{bmatrix} x \\ x' \end{bmatrix} \right) \Rightarrow \frac{\partial V}{\partial x} f(x, u) + \frac{\partial V}{\partial x'} f(x', u) \leq -\kappa V(x, x'), \end{aligned}$$

for any $x, x' \in \mathbb{R}^n$, any $u \in U$, some \mathcal{K}_∞ functions $\underline{\alpha}, \overline{\alpha}$ and some $\kappa \in \mathbb{R}^+$. Hence, V is a δ_3 -GAS Lyapunov function for Σ . This completes the proof.

Before providing the characterization of δ_3 -ISS in terms of existence of a δ_3 -ISS Lyapunov function, we need the following technical lemma, inspired by Proposition 5.3 in [1]. By following similar steps as in [1], we need to define the proximal point function $\text{sat}_U : \mathbb{R}^m \rightarrow U$, defined by:

$$\text{sat}_U(u) = \arg \min_{u' \in U} \|u' - u\|. \quad (3.10)$$

As explained in [1], by assuming U is closed and convex and since $\|\cdot\| : \mathbb{R}^m \rightarrow \mathbb{R}_0^+$ is a proper and convex function, the definition (3.10) is well-defined and the minimizer of $\|u' - u\|$ with $u' \in U$ is unique. Moreover, by convexity of U we have:

$$\|\text{sat}_U(u_1) - \text{sat}_U(u_2)\| \leq \|u_1 - u_2\|, \quad \forall u_1, u_2 \in \mathbb{R}^m. \quad (3.11)$$

Lemma 3.7. Consider a control system $\Sigma = (\mathbb{R}^n, U, \mathcal{U}, f)$, where U is closed and convex. If Σ is δ_3 -ISS, equipped with a metric \mathbf{d} such that $\psi(\cdot) = \mathbf{d}(\cdot, y)$ is continuous⁴ for any $y \in \mathbb{R}^n$, then there exists a \mathcal{K}_∞ function ρ such that the control system $\widehat{\Sigma} = (\mathbb{R}^{2n}, D, \mathcal{D}, \widehat{f})$ ⁵ is U_3 GAS with respect to the diagonal set Δ , where:

$$\widehat{f}(\zeta, \omega) = \begin{bmatrix} f(\xi_1, \text{sat}_U(\omega_1 + \rho(\mathbf{d}(\xi_1, \xi_2))\omega_2)) \\ f(\xi_2, \text{sat}_U(\omega_1 - \rho(\mathbf{d}(\xi_1, \xi_2))\omega_2)) \end{bmatrix},$$

$$\zeta = [\xi_1^T, \xi_2^T]^T, D = U \times \mathcal{B}_1(0_m), \text{ and } \omega = [\omega_1^T, \omega_2^T]^T.$$

Proof. The proof was inspired by the proof of Proposition 5.3 in [1]. We include the complete details of the proof to ensure that the interested reader can assess the essential differences caused by using the arbitrary metric \mathbf{d} rather than the Euclidean metric. Since Σ is δ_3 -ISS, equipped with the metric \mathbf{d} , there exist some $\mathcal{K}\mathcal{L}$ function β and \mathcal{K}_∞ function γ such that:

$$\mathbf{d}(\xi_{xv}(t), \xi_{x'v'}(t)) \leq \max\{\beta(\mathbf{d}(x, x'), t), \gamma(\|v - v'\|_\infty)\}. \quad (3.12)$$

Note that, inequality (3.12) is a straightforward consequence of inequality (2.2) in Definition 2.3 (see Remark 2.5 in [33]). Using the results in Lemma 3.5 and the proposed metric $\widehat{\mathbf{d}}$ in (3.6), we have that $\mathbf{d}(x, x') = \widehat{\mathbf{d}}(z, \Delta)$, where $z = [x^T, x'^T]^T$. Without loss of generality we can assume $\alpha(r) = \beta(r, 0) > r$ for any $r \in \mathbb{R}^+$.

Let ρ be a \mathcal{K}_∞ function satisfying $\rho(r) \leq \frac{1}{2}\gamma^{-1} \circ (\alpha^{-1}(r)/4)$ (note that $\gamma, \alpha \in \mathcal{K}_\infty$). Now we show that

$$\gamma(\|2\omega_2(t)\rho(\widehat{\mathbf{d}}(\zeta_{z\omega}(t), \Delta))\|) \leq \widehat{\mathbf{d}}(z, \Delta)/2, \quad (3.13)$$

for any $t \in \mathbb{R}_0^+$, any $z \in \mathbb{R}^{2n}$, and any $\omega = [\omega_1^T, \omega_2^T]^T \in \mathcal{D}$. Since γ is a \mathcal{K}_∞ function and $\omega_2(t) \in \mathcal{B}_1(0_m)$ for any $t \in \mathbb{R}_0^+$, it is enough to show

$$\gamma(2\rho(\widehat{\mathbf{d}}(\zeta_{z\omega}(t), \Delta))) \leq \widehat{\mathbf{d}}(z, \Delta)/2. \quad (3.14)$$

Since

$$\begin{aligned} \gamma(2\rho(\widehat{\mathbf{d}}(\zeta_{z\omega}(0), \Delta))) &= \gamma(2\rho(\widehat{\mathbf{d}}(z, \Delta))) \\ &\leq \alpha^{-1}(\widehat{\mathbf{d}}(z, \Delta))/4 < \widehat{\mathbf{d}}(z, \Delta)/4, \end{aligned}$$

and $\varphi(\cdot) = \widehat{\mathbf{d}}(\cdot, \Delta)$ is a continuous⁴ function (see proof of Theorem 3.4), then for all $t \in \mathbb{R}_0^+$ small enough, we have $\gamma(2\rho(\widehat{\mathbf{d}}(\zeta_{z\omega}(t), \Delta))) \leq \widehat{\mathbf{d}}(z, \Delta)/4$. Now, let

$$t_1 = \inf\{t > 0 \mid \gamma(2\rho(\widehat{\mathbf{d}}(\zeta_{z\omega}(t), \Delta))) > \widehat{\mathbf{d}}(z, \Delta)/2\}.$$

Clearly $t_1 > 0$. We will show that $t_1 = \infty$. Now, assume by contradiction that $t_1 < \infty$. Therefore, the inequality (3.14) holds for all $t \in [0, t_1)$. Hence, for all $t \in [0, t_1)$, one obtains:

$$\begin{aligned} \gamma(\|2\omega_2(t)\rho(\widehat{\mathbf{d}}(\zeta_{z\omega}(t), \Delta))\|) &\leq \gamma(2\rho(\widehat{\mathbf{d}}(\zeta_{z\omega}(t), \Delta))) \\ &\leq \widehat{\mathbf{d}}(z, \Delta)/2 < \alpha(\widehat{\mathbf{d}}(z, \Delta))/2. \end{aligned} \quad (3.15)$$

Let v and v' be defined as:

$$\begin{aligned} v(t) &= \text{sat}_U(\omega_1(t) + \rho(\widehat{\mathbf{d}}(\zeta_{z\omega}(t), \Delta))\omega_2(t)), \\ v'(t) &= \text{sat}_U(\omega_1(t) - \rho(\widehat{\mathbf{d}}(\zeta_{z\omega}(t), \Delta))\omega_2(t)). \end{aligned}$$

By using (3.11), we obtain:

$$\|v(t) - v'(t)\| \leq \|2\omega_2(t)\rho(\widehat{\mathbf{d}}(\zeta_{z\omega}(t), \Delta))\|.$$

Using (3.12) and (3.15), we have:

$$\begin{aligned} \widehat{\mathbf{d}}(\zeta_{z\omega}(t), \Delta) &= \mathbf{d}(\xi_{xv}(t), \xi_{x'v'}(t)) \leq \beta(\mathbf{d}(x, x'), 0) \\ &= \beta(\widehat{\mathbf{d}}(z, \Delta), 0) = \alpha(\widehat{\mathbf{d}}(z, \Delta)), \end{aligned} \quad (3.16)$$

for any $t \in [0, t_1)$, any $\omega \in \mathcal{D}$, and any $z = [x^T, x'^T]^T \in \mathbb{R}^{2n}$. Using $\rho(r) \leq \frac{1}{2}\gamma^{-1} \circ (\alpha^{-1}(r)/4)$, the inequality (3.16) implies that

$$\gamma(2\rho(\widehat{\mathbf{d}}(\zeta_{z\omega}(t), \Delta))) \leq \widehat{\mathbf{d}}(z, \Delta)/4, \quad (3.17)$$

for any $t \in [0, t_1)$. Since the function $\psi(\cdot) = \widehat{\mathbf{d}}(\cdot, \Delta)$ is continuous⁴, the inequality (3.17) contradicts the definition of t_1 . Therefore, $t_1 = \infty$ and inequality (3.13) is proved for all $t \in \mathbb{R}_0^+$. Therefore, using (3.12) and (3.13), we obtain:

$$\begin{aligned} \widehat{\mathbf{d}}(\zeta_{z\omega}(t), \Delta) &= \mathbf{d}(\xi_{xv}(t), \xi_{x'v'}(t)) \\ &\leq \max\{\beta(\mathbf{d}(x, x'), t), \gamma(\|v - v'\|_\infty)\} \\ &\leq \max\{\beta(\mathbf{d}(x, x'), t), \gamma(\|2\omega_2(t)\rho(\widehat{\mathbf{d}}(\zeta_{z\omega}(t), \Delta))\|_\infty)\} \\ &\leq \max\{\beta(\widehat{\mathbf{d}}(z, \Delta), t), \widehat{\mathbf{d}}(z, \Delta)/2\}, \end{aligned}$$

for any $z = [x^T, x'^T]^T \in \mathbb{R}^{2n}$, any $\omega \in \mathcal{D}$, and any $t \in \mathbb{R}_0^+$. Since β is a $\mathcal{K}\mathcal{L}$ function, it can be readily seen that for each $r > 0$ if $\widehat{\mathbf{d}}(z, \Delta) \leq r$, then there exists some $T_r \geq 0$ such that for any $t \geq T_r$, $\beta(\widehat{\mathbf{d}}(z, \Delta), t) \leq r/2$ and, hence, $\widehat{\mathbf{d}}(\zeta_{z\omega}(t), \Delta) \leq r/2$. Now we show that the set Δ is a global attractor for the control system $\widehat{\Sigma}$. For any $\varepsilon \in \mathbb{R}^+$, let k be a positive integer such that $2^{-k}r < \varepsilon$. Let $r_1 = r$ and $r_i = r_{i-1}/2$ for $i \geq 2$, and let $\tau = T_{r_1} + T_{r_2} + \dots + T_{r_k}$. Then, for $t \geq \tau$, we have $\widehat{\mathbf{d}}(\zeta_{z\omega}(t), \Delta) \leq 2^{-k}r < \varepsilon$ for all $\widehat{\mathbf{d}}(z, \Delta) \leq r$, and all $\omega \in \mathcal{D}$. Therefore, it can be concluded that the set Δ is a uniform global attractor for the control system $\widehat{\Sigma}$.

⁵ \mathcal{D} is the set of all measurable and locally essentially bounded functions of time from intervals of the form $]a, b[\subseteq \mathbb{R}$ to D with $a < 0$ and $b > 0$.

Furthermore, since $\widehat{\mathbf{d}}(\xi_{z\omega}(t), \Delta) \leq \beta(\widehat{\mathbf{d}}(z, \Delta), 0)$ for all $t \in \mathbb{R}_0^+$, all $z \in \mathbb{R}^{2n}$, and all $\omega \in \mathcal{D}$, the control system $\widehat{\Sigma}$ is uniformly globally stable and as shown in [36], it is U_3 GAS.

Finally, the next theorem provides a characterization of δ_3 -ISS in terms of the existence of a δ_3 -ISS Lyapunov function.

Theorem 3.8. Consider a control system $\Sigma = (\mathbb{R}^n, \mathcal{U}, f)$. If \mathcal{U} is compact and convex and \mathbf{d} is a metric such that the function $\psi(\cdot) = \mathbf{d}(\cdot, y)$ is continuous⁴ for any $y \in \mathbb{R}^n$ then the following statements are equivalent:

- (1) Σ is forward complete and there exists a δ_3 -ISS Lyapunov function, equipped with metric \mathbf{d} .
- (2) Σ is δ_3 -ISS, equipped with metric \mathbf{d} .

Proof. The proof from (1) to (2) has been shown in Theorem 2.6 in [3], even in the absence of the compactness and convexity assumptions on \mathcal{U} and the continuity assumption on \mathbf{d} . We now prove that (2) implies (1). As we proved in Lemma 3.7, since Σ is δ_3 -ISS, it implies that the control system $\widehat{\Sigma}$, defined in Lemma 3.7, is U_3 GAS with respect to Δ . Since $\psi(\cdot) = \mathbf{d}(\cdot, y)$ is continuous⁴ for any $y \in \mathbb{R}^n$, it can be easily verified that $\widehat{\psi}(\cdot) = \widehat{\mathbf{d}}(\cdot, z')$ is continuous⁴ for any $z' \in \mathbb{R}^{2n}$, where the metric $\widehat{\mathbf{d}}$ was defined in the proof of Lemma 3.5. Using Theorem 3.4, we conclude that there exists a U_3 GAS Lyapunov function V , with respect to Δ , for $\widehat{\Sigma}$. By using the special form of $\widehat{\Sigma}$, defined in Lemma 3.7, the equality (3.9), and slightly abusing notation the function V satisfies:

$$(i) \quad \underline{\alpha} \left(\widehat{\mathbf{d}} \left(\begin{bmatrix} x \\ x' \end{bmatrix}, \Delta \right) \right) \leq V \left(\begin{bmatrix} x \\ x' \end{bmatrix} \right) \leq \overline{\alpha} \left(\widehat{\mathbf{d}} \left(\begin{bmatrix} x \\ x' \end{bmatrix}, \Delta \right) \right) \Rightarrow \underline{\alpha}(\mathbf{d}(x, x')) \leq V(x, x') \leq \overline{\alpha}(\mathbf{d}(x, x'));$$

for any $x, x' \in \mathbb{R}^n$, some \mathcal{K}_∞ functions $\underline{\alpha}, \overline{\alpha}$ and

$$(ii) \quad \begin{aligned} & \left[\frac{\partial V}{\partial x} \frac{\partial V}{\partial x'} \right] \begin{bmatrix} f(x, \text{sat}_{\mathcal{U}}(d_1 + \rho(\mathbf{d}(x, x'))d_2)) \\ f(x', \text{sat}_{\mathcal{U}}(d_1 - \rho(\mathbf{d}(x, x'))d_2)) \end{bmatrix} \\ & \leq -\kappa V \left(\begin{bmatrix} x \\ x' \end{bmatrix} \right) \\ & \Rightarrow \frac{\partial V}{\partial x} f(x, \text{sat}_{\mathcal{U}}(d_1 + \rho(\mathbf{d}(x, x'))d_2)) \\ & \quad + \frac{\partial V}{\partial x'} f(x', \text{sat}_{\mathcal{U}}(d_1 - \rho(\mathbf{d}(x, x'))d_2)) \\ & \leq -\kappa V(x, x'), \end{aligned} \quad (3.18)$$

for some $\kappa \in \mathbb{R}^+$, any $x, x' \in \mathbb{R}^n$, and any $[d_1^T, d_2^T]^T \in \mathcal{D}$. By choosing $d_1 = (u + u')/2$ and $d_2 = (u - u')/(2\rho(\mathbf{d}(x, x')))$ for any $u, u' \in \mathcal{U}$, it can be readily checked that $[d_1^T, d_2^T]^T \in \mathcal{U} \times \mathcal{B}_1(0_m)$, whenever $2\rho(\mathbf{d}(x, x')) \geq \|u - u'\|$. Hence, using (3.18), we have that the following implication holds:

if $\varphi(\mathbf{d}(x, x')) \geq \|u - u'\|$, then

$$\frac{\partial V}{\partial x} f(x, u) + \frac{\partial V}{\partial x'} f(x', u') \leq -\kappa V(x, x'), \quad (3.19)$$

where $\varphi(r) = 2\rho(r)$. As shown in Remark 2.4 in [33], there is no loss of generality in modifying inequalities (3.19) to

$$\frac{\partial V}{\partial x} f(x, u) + \frac{\partial V}{\partial x'} f(x', u') \leq -\widehat{\kappa} V(x, x') + \sigma(\|u - u'\|),$$

for some \mathcal{K}_∞ function σ and some $\widehat{\kappa} \in \mathbb{R}^+$, which completes the proof.

3.2. Contraction metrics description

In addition to incremental Lyapunov functions, the δ_3 -GAS and δ_3 -ISS conditions can be checked by resorting to contraction

metrics. The interested reader may consult [37] for more detailed information about the notion of contraction metrics. Note that, for all definitions and results in this subsection we require function f to be continuously differentiable which was not the case in the characterizations of incremental stability using incremental Lyapunov functions.

Now we recall the notions of contraction metrics, presented in [37,2].

Definition 3.9 ([37]). Let $\Sigma = (\mathbb{R}^n, \mathcal{U}, f)$ be a smooth control system on \mathbb{R}^n equipped with a Riemannian metric G . The metric G is said to be a contraction metric, with respect to states, for system Σ if there exists some $\widehat{\lambda} \in \mathbb{R}^+$ such that:

$$\langle X, X \rangle_F \leq -\widehat{\lambda} \langle X, X \rangle_G, \quad (3.20)$$

for $F(x, u) = \left(\frac{\partial f}{\partial x} \right)^T G(x) + G(x) \frac{\partial f}{\partial x} + \frac{\partial G}{\partial x} f(x, u)$, any $u \in \mathcal{U}, x \in \mathbb{R}^n$, and $x \in \mathbb{R}^n$. The constant $\widehat{\lambda}$ is called the contraction rate.

Note that when the metric G is constant, the condition (3.20) is known as the Demidovich's condition [15,38,39]. It is shown in [15] that such condition implies δ -GAS and the convergent system property for Σ .

Definition 3.10 ([2]). Let $\Sigma = (\mathbb{R}^n, \mathcal{U}, f)$ be a smooth control system on \mathbb{R}^n equipped with a Riemannian metric G . The metric G is said to be a contraction metric, with respect to states and inputs, for system Σ if there exist some $\widehat{\lambda} \in \mathbb{R}^+$ and $\alpha \in \mathbb{R}_0^+$ such that:

$$\langle X, X \rangle_F + 2 \left\langle \frac{\partial f}{\partial u} Y, X \right\rangle_G \leq -\widehat{\lambda} \langle X, X \rangle_G + \alpha \langle X, X \rangle_G^{\frac{1}{2}} \langle Y, Y \rangle_m^{\frac{1}{2}}, \quad (3.21)$$

for $F(x, u) = \left(\frac{\partial f}{\partial x} \right)^T G(x) + G(x) \frac{\partial f}{\partial x} + \frac{\partial G}{\partial x} f(x, u)$, any $X \in \mathbb{R}^n, x \in \mathbb{R}^n$, $u \in \mathcal{U}$, and $Y \in \mathbb{R}^m$. The constant $\widehat{\lambda}$ is called the contraction rate.

The following theorem shows that the existence of a contraction metric, with respect to states and inputs, (resp. with respect to states) implies δ_3 -ISS (resp. δ_3 -GAS).

Theorem 3.11. Let $\Sigma = (\mathbb{R}^n, \mathcal{U}, f)$ be a smooth control system on \mathbb{R}^n equipped with a Riemannian metric G and let \mathcal{U} be a convex set. If the metric G is a contraction metric, with respect to states and inputs, (resp. with respect to states) for system Σ and $(\mathbb{R}^n, \mathbf{d}_G)$ is a complete metric space, then Σ is δ_3 -ISS (resp. δ_3 -GAS).

Proof. Since $(\mathbb{R}^n, \mathbf{d}_G)$ is a complete metric space, using the Hopf–Rinow theorem [40], we conclude that \mathbb{R}^n with respect to the metric G is geodesically complete. The rest of the proof is inspired by the proof of Theorem 2 in [4]. Consider two points x and x' in \mathbb{R}^n and a geodesic $\chi : [0, 1] \rightarrow \mathbb{R}^n$ joining $x = \chi(0)$ and $x' = \chi(1)$. The geodesic distance between the points x and x' is given by:

$$\mathbf{d}_G(x, x') = \int_0^1 \sqrt{\left(\frac{d\chi(s)}{ds} \right)^T G(\chi(s)) \frac{d\chi(s)}{ds}} ds. \quad (3.22)$$

Consider the straight line $\widehat{\chi}_t(s) = (1-s)v(t) + sv'(t)$, for fixed $t \in \mathbb{R}_0^+$, fixed $v, v' \in \mathcal{U}$, and for any $s \in [0, 1]$. The curve $\widehat{\chi}_t$ is a geodesic, with respect to the Euclidean metric, on the subset $\mathcal{U} \subseteq \mathbb{R}^m$ joining $v(t) = \widehat{\chi}_t(0)$ and $v'(t) = \widehat{\chi}_t(1)$. Consider also the input curve v_s defined by $v_s(t) = \widehat{\chi}_t(s)$. Let $l(t)$ be the length of the curve $\xi_{\chi(s)v_s(t)}$ parametrized by s and with respect to the metric G , i.e.:

$$l(t) = \int_0^1 \sqrt{\delta \xi^T G(\xi_{\chi(s)v_s(t)}) \delta \xi} ds, \quad (3.23)$$

with $\delta \xi = \frac{\partial}{\partial s} \xi_{\chi(s)v_s(t)}$.

In the rest of the proof, we drop the argument of the metric G for the sake of simplicity. By taking the derivative of (3.23) with respect to time, we obtain:

$$\begin{aligned} \frac{d}{dt}l(t) &= \int_0^1 \frac{\frac{d}{dt}(\delta \xi^T G \delta \xi)}{2\sqrt{\delta \xi^T G \delta \xi}} ds \\ &= \int_0^1 \frac{\delta \xi^T \left(\left(\frac{\partial f}{\partial x} \right)^T G + \frac{\partial G}{\partial x} f + G \frac{\partial f}{\partial x} \right) \delta \xi + 2\delta v^T \left(\frac{\partial f}{\partial u} \right)^T G \delta \xi}{2\sqrt{\delta \xi^T G \delta \xi}} ds, \end{aligned}$$

where $\delta v = \frac{\partial}{\partial s} v_s(t)$.

Since G is a contraction metric, with respect to states and inputs, with $\hat{\lambda}$ and α the constants introduced in Definition 3.10, the following inequality holds:

$$\begin{aligned} \frac{d}{dt}l(t) &\leq -\frac{\hat{\lambda}}{2}l(t) + \frac{\alpha}{2} \int_0^1 \sqrt{\delta v^T \delta v} ds \\ &= -\frac{\hat{\lambda}}{2}l(t) + \frac{\alpha}{2} \|v(t) - v'(t)\|. \end{aligned} \quad (3.24)$$

Using (3.24) and the comparison principle [41], we obtain:

$$\begin{aligned} l(t) &\leq e^{-\frac{\hat{\lambda}}{2}t} l(0) + \frac{\alpha}{2} e^{-\frac{\hat{\lambda}}{2}t} * \|v(t) - v'(t)\| \\ &\leq e^{-\frac{\hat{\lambda}}{2}t} l(0) + \frac{\alpha}{\hat{\lambda}} \left(1 - e^{-\frac{\hat{\lambda}}{2}t}\right) \|v - v'\|_{\infty} \\ &\leq e^{-\frac{\hat{\lambda}}{2}t} l(0) + \frac{\alpha}{\hat{\lambda}} \|v - v'\|_{\infty}, \end{aligned}$$

where $*$ denotes the convolution integral.⁶ From (3.22) and (3.23), it can be seen that $l(0) = \mathbf{d}_G(x, x')$. However, for $t \in \mathbb{R}^+$, $l(t)$ is not necessarily the Riemannian distance function, determined by G , because $\xi_{\chi(s)v_s}(t)$ is not necessarily a geodesic, implying that it is always bigger than or equal to the Riemannian distance function⁷: $\mathbf{d}_G(\xi_{xv}(t), \xi_{x'v'}(t)) \leq l(t)$, and, hence, the following inequality holds:

$$\mathbf{d}_G(\xi_{xv}(t), \xi_{x'v'}(t)) \leq e^{-\frac{\hat{\lambda}}{2}t} \mathbf{d}_G(x, x') + \frac{\alpha}{\hat{\lambda}} \|v - v'\|_{\infty},$$

which, in turn, implies that Σ is δ_3 -ISS. The proof for the case that G is a contraction metric, with respect to states, can be readily verified by just enforcing $\delta v(t) = 0$ and $v(t) = v'(t)$ for any $t \in \mathbb{R}_0^+$.

Since completeness of the metric space $(\mathbb{R}^n, \mathbf{d}_G)$ is crucial to the previous proof, the following lemma provides a sufficient condition on the metric G guaranteeing that $(\mathbb{R}^n, \mathbf{d}_G)$ is a complete metric space.

Lemma 3.12. *The Riemannian manifold \mathbb{R}^n equipped with a Riemannian metric G , satisfying⁸ $\bar{\omega} \|y\|^2 \leq y^T G(x)y$ for any $x, y \in \mathbb{R}^n$ and for some positive constant $\bar{\omega}$, is complete as a metric space, with respect to \mathbf{d}_G .*

Proof. The proof was suggested to us by C. Manolescu. First, for each pair of points $x, y \in \mathbb{R}^n$ we define the path space:

$$\begin{aligned} \Omega(x, y) &= \{\chi : [0, 1] \rightarrow \mathbb{R}^n \mid \chi \text{ is piecewise smooth,} \\ &\quad \chi(0) = x, \text{ and } \chi(1) = y\}. \end{aligned}$$

Recall that a function $\chi : [a, b] \rightarrow \mathbb{R}^n$ is piecewise smooth if χ is continuous and if there exists a partitioning $a = a_1 < a_2 < \dots <$

$a_k = b$ of $[a, b]$ such that $\chi|_{(a_i, a_{i+1})}$ is smooth for $i = 1, \dots, k-1$. We can then define the Riemannian distance function $\mathbf{d}_G(x, y)$ between points $x, y \in \mathbb{R}^n$ as

$$\mathbf{d}_G(x, y) = \inf_{\chi \in \Omega(x, y)} \int_0^1 \sqrt{\left(\frac{d\chi(s)}{ds} \right)^T G(\chi(s)) \frac{d\chi(s)}{ds}} ds.$$

It follows immediately that \mathbf{d}_G is a metric on \mathbb{R}^n . The Riemannian manifold \mathbb{R}^n is a complete metric space, equipped with the metric \mathbf{d}_G , if every Cauchy sequence⁹ of points in \mathbb{R}^n has a limit in \mathbb{R}^n . Assume $\{x_n\}_{n=1}^{\infty}$ is a Cauchy sequence in \mathbb{R}^n , equipped with the metric \mathbf{d}_G . By using the assumption on G , we have

$$\begin{aligned} \mathbf{d}_G(x_n, x_m) &= \inf_{\chi \in \Omega(x_n, x_m)} \int_0^1 \sqrt{\left(\frac{d\chi(s)}{ds} \right)^T G(\chi(s)) \frac{d\chi(s)}{ds}} ds \\ &\geq \sqrt{\bar{\omega}} \inf_{\chi \in \Omega(x_n, x_m)} \int_0^1 \sqrt{\left(\frac{d\chi(s)}{ds} \right)^T \frac{d\chi(s)}{ds}} ds \\ &= \sqrt{\bar{\omega}} \|x_n - x_m\|. \end{aligned} \quad (3.25)$$

It is readily seen from the inequality (3.25) that the sequence $\{x_n\}_{n=1}^{\infty}$ is also a Cauchy sequence in \mathbb{R}^n with respect to the Euclidean metric. Since the Riemannian manifold \mathbb{R}^n with respect to the Euclidean metric is a complete metric space, the sequence $\{x_n\}_{n=1}^{\infty}$ converges to a point, named x^* , in \mathbb{R}^n . By picking a convex compact subset $D \subset \mathbb{R}^n$, containing x^* , and using Lemma 8.18 in [30], we have: $\bar{\omega} \|y\|^2 \geq y^T G(x)y$ for any $y \in \mathbb{R}^n, x \in D$, and some positive constant $\bar{\omega}$. Since the sequence $\{x_n\}_{n=1}^{\infty}$ converges to $x^* \in D$, there exists some integer N such that the sequence $\{x_n\}_{n=N}^{\infty}$ remains forever inside D . Hence, we have:

$$\sqrt{\bar{\omega}} \|x_n - x^*\| \leq \mathbf{d}_G(x_n, x^*) \leq \sqrt{\bar{\omega}} \|x_n - x^*\|,$$

for any $n > N$. Therefore, the sequence $\{x_n\}_{n=1}^{\infty}$ converges to $x^* \in \mathbb{R}^n$, equipped with the metric \mathbf{d}_G . Therefore, \mathbb{R}^n with respect to the metric \mathbf{d}_G is a complete metric space.

Resuming, in this section we have provided a characterization of δ_3 -GAS and δ_3 -ISS in terms of the existence of δ_3 -GAS and δ_3 -ISS Lyapunov functions and we have provided sufficient conditions for δ_3 -GAS and δ_3 -ISS in terms of the existence of a contraction metric. Based on these results, in the next section, we propose a backstepping controller design procedure, providing controllers rendering control systems incrementally stable. Additionally, we will provide incremental Lyapunov functions and contraction metrics (the latter for smooth control systems).

4. Backstepping design procedure

The backstepping method proposed here is inspired by the backstepping method, described in [15,18]. Here, we will extend this approach to render the closed-loop system δ_3 -ISS and to construct δ_3 -ISS Lyapunov functions. Consider the following subclass of control systems:

$$\Sigma : \begin{cases} \dot{\eta} = f(\eta, \zeta), \\ \dot{\zeta} = v, \end{cases} \quad (4.1)$$

where $x = [y^T, z^T]^T \in \mathbb{R}^{n_\eta+n_\zeta}$ is the state of Σ , y and z are initial conditions for η, ζ -subsystems, respectively, and v is the control input.

In support of the main result of this section (Theorem 4.2), we need the following technical result.

⁶ $e^{-\frac{\hat{\lambda}}{2}t} * \|v(t) - v'(t)\| = \int_0^t e^{-\frac{\hat{\lambda}}{2}(t-\tau)} \|v(\tau) - v'(\tau)\| d\tau$.

⁷ Note that given a Riemannian metric G , the Riemannian distance function is the smallest distance, determined by G .

⁸ This condition is nothing more than uniform positive definiteness of G .

⁹ A sequence $\{x_n\}_{n=1}^{\infty}$ in a metric space X , equipped with a metric \mathbf{d} , is a Cauchy sequence if $\lim_{n,m \rightarrow \infty} \mathbf{d}(x_n, x_m) = 0$.

Lemma 4.1. Consider the following interconnected control system

$$\Sigma : \begin{cases} \dot{\eta} = f(\eta, \zeta, v), \\ \dot{\zeta} = g(\zeta, v). \end{cases} \quad (4.2)$$

Let the η -subsystem be δ_3 -ISS with respect to ζ, v , as inputs, and let the ζ -subsystem be δ_3 -ISS with respect to v for some metrics \mathbf{d}_η and \mathbf{d}_ζ , respectively, such that the solutions $\eta_{y\zeta v}$ ¹⁰ and ζ_{zv} satisfy the following inequalities:

$$\mathbf{d}_\eta(\eta_{y\zeta v}(t), \eta_{y'\zeta'v'}(t)) \leq \beta_\eta(\mathbf{d}_\eta(y, y'), t) + \gamma_\zeta(\mathbf{d}_\zeta(\zeta, \zeta')_\infty) + \gamma_v(\|v - v'\|_\infty), \quad (4.3)$$

$$\mathbf{d}_\zeta(\zeta_{zv}(t), \zeta_{z'v'}(t)) \leq \beta_\zeta(\mathbf{d}_\zeta(z, z'), t) + \tilde{\gamma}_v(\|v - v'\|_\infty), \quad (4.4)$$

where y, y' and z, z' are the initial conditions for the η, ζ -subsystems, respectively. Then, the interconnected control system Σ in (4.2) is δ_3 -ISS with respect to v .

The proof of the preceding result can be found in the Appendix and is inspired by the proof of Proposition 4.7 in [1].

We can now state the main result of this section, on a backstepping controller design approach for the control system Σ in (4.1), rendering the resulting closed-loop system δ_3 -ISS.

Theorem 4.2. Consider the control system Σ of the form (4.1). Suppose there exists a continuously differentiable function $\psi : \mathbb{R}^{n_\eta} \rightarrow \mathbb{R}^{n_\zeta}$ such that the control system

$$\Sigma_\eta : \dot{\eta} = f(\eta, \psi(\eta) + \tilde{v}) \quad (4.5)$$

is δ_3 -ISS with respect to the input \tilde{v} . Then for any $\lambda \in \mathbb{R}^+$, the state feedback control law:

$$v = k(\eta, \zeta, \hat{v}) = -\lambda(\zeta - \psi(\eta)) + \frac{\partial \psi}{\partial y}(\eta)f(\eta, \zeta) + \hat{v} \quad (4.6)$$

renders the control system $\Sigma \delta_3$ -ISS with respect to the input \hat{v} .

Proof. Consider the following coordinate transformation:

$$\chi = \begin{bmatrix} \chi_1 \\ \chi_2 \end{bmatrix} = \phi(\xi) = \begin{bmatrix} \eta \\ \zeta - \psi(\eta) \end{bmatrix}, \quad (4.7)$$

where $\xi = [\eta^T, \zeta^T]^T$. In the new coordinate χ , we obtain the following dynamics:

$$\hat{\Sigma} : \begin{cases} \dot{\chi}_1 = f(\chi_1, \psi(\chi_1) + \chi_2), \\ \dot{\chi}_2 = v - \frac{\partial \psi}{\partial y}(\chi_1)f(\chi_1, \psi(\chi_1) + \chi_2). \end{cases}$$

The proposed control law (4.6), given in the new coordinate χ by

$$\begin{aligned} v &= k(\chi_1, \chi_2 + \psi(\chi_1), \hat{v}) \\ &= -\lambda\chi_2 + \frac{\partial \psi}{\partial y}(\chi_1)f(\chi_1, \psi(\chi_1) + \chi_2) + \hat{v}, \end{aligned} \quad (4.8)$$

transforms the control system $\hat{\Sigma}$ into:

$$\tilde{\Sigma} : \begin{cases} \dot{\chi}_1 = f(\chi_1, \psi(\chi_1) + \chi_2), \\ \dot{\chi}_2 = -\lambda\chi_2 + \hat{v}. \end{cases} \quad (4.9)$$

Due to the choice of ψ , the χ_1 -subsystem of $\tilde{\Sigma}$ is δ_3 -ISS with respect to χ_2 . It can be easily verified that the χ_2 -subsystem is input-to-state stable with respect to the input \hat{v} . Since any ISS linear

control system is also δ -ISS [1], χ_2 -subsystem is also δ -ISS¹¹ with respect to \hat{v} . Therefore, using Lemma 4.1, we conclude that the control system $\tilde{\Sigma}$ is δ_3 -ISS with respect to the input \hat{v} . Since, δ_3 -ISS property is coordinate invariant [2], we conclude that the original control system Σ in (4.1) equipped with the state feedback control law in (4.6) is δ_3 -ISS with respect to the input \hat{v} which completes the proof.

Remark 4.3. The δ_3 -ISS property of system Σ_η in (4.5) can be established, for example, using the approaches provided in [15,17] for some relevant classes of control systems (such as piece-wise affine systems and Lur'e-type systems).

Remark 4.4. We should emphasize that incremental stability requires the uniform asymptotic stability of every trajectory and can, in general, not be achieved by just asymptotically stabilizing a particular time-varying trajectory using conventional techniques. For instance, the first example in [22], see also [23], illustrates a two-dimensional nonlinear system which is globally uniformly convergent, i.e. exhibits a uniformly globally asymptotically stable trajectory, but it is not globally incrementally stable. Hence, the induction of incremental stability by means of feedback requires different controller synthesis techniques, such as e.g. the proposed one here.

Remark 4.5. The result of Theorem 4.2 can be extended to the case that we have arbitrary number of integrators:

$$\Sigma : \begin{cases} \dot{\eta} = f(\eta, \zeta_1), \\ \dot{\zeta}_1 = \zeta_2, \\ \vdots \\ \dot{\zeta}_k = v. \end{cases}$$

Note that in this case, the functions f and ψ must be sufficiently differentiable.

Although the proposed approach in Theorem 4.2 provides a controller rendering the control system Σ of the form (4.1) δ_3 -ISS, it does not provide a way of constructing δ_3 -ISS Lyapunov functions or contraction metrics. In the next lemmas, we show how to construct incremental Lyapunov functions and contraction metrics for the resulting closed-loop system, recursively. Note that the constructed incremental Lyapunov functions can be used as a necessary tool in the analysis in [11,24,26,28]. We will show in the example section how the explicit availability of an incremental Lyapunov function helps us to use the results in [11] to construct a finite bisimilar abstraction for an incrementally input-to-state stable (non-smooth) control system.

Lemma 4.6. Consider the control system Σ of the form (4.1). Suppose there exists a continuously differentiable function $\psi : \mathbb{R}^{n_\eta} \rightarrow \mathbb{R}^{n_\zeta}$ such that the smooth function $\hat{V} : \mathbb{R}^{n_\eta} \times \mathbb{R}^{n_\eta} \rightarrow \mathbb{R}_0^+$ is a δ_3 -ISS Lyapunov function for the control system

$$\Sigma_\eta : \dot{\eta} = f(\eta, \psi(\eta) + \tilde{v}), \quad (4.10)$$

and with respect to the control input \tilde{v} . Assume that \hat{V} satisfies condition (iii) in Definition 3.1 for some $\kappa \in \mathbb{R}^+$ and some $\sigma \in \mathcal{K}_\infty$, satisfying $\sigma(r) \leq \hat{\kappa}r^2$ for some $\hat{\kappa} \in \mathbb{R}^+$ and any $r \in \mathbb{R}_0^+$. Then the function $\tilde{V} : \mathbb{R}^{n_\eta+n_\zeta} \times \mathbb{R}^{n_\eta+n_\zeta} \rightarrow \mathbb{R}_0^+$, defined as

$$\tilde{V}(x, x') = \hat{V}(y, y') + \|(z - \psi(y)) - (z' - \psi(y'))\|^2,$$

where $x = [y^T, z^T]^T$ and $x' = [y'^T, z'^T]^T$, is a δ_3 -ISS Lyapunov function for $\tilde{\Sigma}$ as in (4.1) equipped with the state feedback control law (4.6) for all $\lambda \geq \frac{\kappa+\hat{\kappa}+1}{2}$.

¹⁰ Notation $\eta_{y\zeta v}$ denotes a trajectory of η -subsystem under the inputs ζ and v from initial condition $y \in \mathbb{R}^{n_\eta}$.

¹¹ We recall that δ -ISS property is equivalent to δ_3 -ISS property with respect to the Euclidean metric.

Proof. As explained in the proof of [Theorem 4.2](#), using the proposed state feedback control law (4.6) and the coordinate transformation ϕ in (4.7), the control system Σ of the form (4.1) is transformed to the control system $\tilde{\Sigma}$ in (4.9). Now we show that

$$V(\hat{x}, \hat{x}') = \hat{V}(\hat{x}_1, \hat{x}'_1) + (\hat{x}_2 - \hat{x}'_2)^T (\hat{x}_2 - \hat{x}'_2),$$

is a δ_3 -ISS Lyapunov function for $\tilde{\Sigma}$, where $\hat{x} = [\hat{x}_1^T, \hat{x}_2^T]^T$ and $\hat{x}' = [\hat{x}'_1^T, \hat{x}'_2^T]^T$ are the states of $\tilde{\Sigma}$ and \hat{x}_1, \hat{x}'_1 , and \hat{x}_2, \hat{x}'_2 are the states of χ_1, χ_2 -subsystems, respectively. Since \hat{V} is a δ_3 -ISS Lyapunov function for χ_1 -subsystem when χ_2 is the input, it satisfies condition (i) in [Definition 3.1](#) using a metric \mathbf{d} as follows:

$$\underline{\alpha}(\mathbf{d}(\hat{x}_1, \hat{x}'_1)) \leq \hat{V}(\hat{x}_1, \hat{x}'_1) \leq \bar{\alpha}(\mathbf{d}(\hat{x}_1, \hat{x}'_1)),$$

for some $\underline{\alpha}, \bar{\alpha} \in \mathcal{K}_\infty$. Now we define a new metric $\hat{\mathbf{d}} : \mathbb{R}^{n_\eta+n_\zeta} \times \mathbb{R}^{n_\eta+n_\zeta} \rightarrow \mathbb{R}_0^+$ by

$$\hat{\mathbf{d}}(\hat{x}, \hat{x}') = \mathbf{d}(\hat{x}_1, \hat{x}'_1) + \|\hat{x}_2 - \hat{x}'_2\|. \quad (4.11)$$

It can be readily checked that $\hat{\mathbf{d}}$ satisfies all three conditions of a metric. Using metric $\hat{\mathbf{d}}$, function V satisfies condition (i) in [Definition 3.1](#) as follows:

$$\underline{\mu}(\hat{\mathbf{d}}(\hat{x}, \hat{x}')) \leq V(\hat{x}, \hat{x}') \leq \bar{\mu}(\hat{\mathbf{d}}(\hat{x}, \hat{x}')),$$

where $\underline{\mu}, \bar{\mu} \in \mathcal{K}_\infty$, $\underline{\mu}(\hat{\mathbf{d}}(\hat{x}, \hat{x}')) = \underline{\alpha}(\mathbf{d}(\hat{x}_1, \hat{x}'_1)) + \|\hat{x}_2 - \hat{x}'_2\|^2$, and $\bar{\mu}(\hat{\mathbf{d}}(\hat{x}, \hat{x}')) = \bar{\alpha}(\mathbf{d}(\hat{x}_1, \hat{x}'_1)) + \|\hat{x}_2 - \hat{x}'_2\|^2$. Now we show that V satisfies condition (iii) in [Definition 3.1](#) for $\tilde{\Sigma}$. Since \hat{V} is a δ_3 -ISS Lyapunov function for χ_1 -subsystem when χ_2 is the input, $\lambda \geq \frac{\kappa+\kappa+1}{2}$, $\sigma(r) \leq \hat{\kappa}r^2$, and using the Cauchy Schwarz inequality, we have:

$$\begin{aligned} & \frac{\partial V}{\partial \hat{x}} [f(\hat{x}_1, \psi(\hat{x}_1) + \hat{x}_2)^T, -\lambda \hat{x}_2^T + \hat{u}^T]^T \\ & + \frac{\partial V}{\partial \hat{x}'} [f(\hat{x}'_1, \psi(\hat{x}'_1) + \hat{x}'_2)^T, -\lambda \hat{x}'_2^T + \hat{u}'^T]^T \\ & \leq \frac{\partial \hat{V}}{\partial \hat{x}_1} f(\hat{x}_1, \psi(\hat{x}_1) + \hat{x}_2) + \frac{\partial \hat{V}}{\partial \hat{x}'_1} f(\hat{x}'_1, \psi(\hat{x}'_1) + \hat{x}'_2) \\ & \quad + 2(\hat{x}_2 - \hat{x}'_2)^T (-\lambda \hat{x}_2 + \hat{u}) - 2(\hat{x}_2 - \hat{x}'_2)^T (-\lambda \hat{x}'_2 + \hat{u}') \\ & \leq -\kappa \hat{V}(\hat{x}_1, \hat{x}'_1) + \sigma(\|\hat{x}_2 - \hat{x}'_2\|) \\ & \quad - 2\lambda \|\hat{x}_2 - \hat{x}'_2\|^2 + 2(\hat{x}_2 - \hat{x}'_2)^T (\hat{u} - \hat{u}') \\ & \leq -\kappa \hat{V}(\hat{x}_1, \hat{x}'_1) + \hat{\kappa} \|\hat{x}_2 - \hat{x}'_2\|^2 \\ & \quad - 2\lambda \|\hat{x}_2 - \hat{x}'_2\|^2 + 2\|\hat{x}_2 - \hat{x}'_2\| \|\hat{u} - \hat{u}'\| \\ & \leq -\kappa \hat{V}(\hat{x}_1, \hat{x}'_1) + \hat{\kappa} \|\hat{x}_2 - \hat{x}'_2\|^2 \\ & \quad - 2\lambda \|\hat{x}_2 - \hat{x}'_2\|^2 + \|\hat{x}_2 - \hat{x}'_2\|^2 + \|\hat{u} - \hat{u}'\|^2 \\ & \leq -\kappa V(\hat{x}, \hat{x}') + \|\hat{u} - \hat{u}'\|^2. \end{aligned}$$

The latter inequality implies that V is a δ_3 -ISS Lyapunov function for $\tilde{\Sigma}$. Since δ_3 -ISS Lyapunov functions are coordinate-invariant [3], we conclude that the function $\tilde{V} : \mathbb{R}^{n_\eta+n_\zeta} \times \mathbb{R}^{n_\eta+n_\zeta} \rightarrow \mathbb{R}_0^+$, defined by

$$\begin{aligned} \tilde{V}(x, x') &= V(\phi(x), \phi(x')) \\ &= \hat{V}(y, y') + \|(z - \psi(y)) - (z' - \psi(y'))\|^2, \end{aligned}$$

is a δ_3 -ISS Lyapunov function for Σ , as in (4.1), equipped with the state feedback control law in (4.6).

Remark 4.7. One can use the LMI based results in [15–17] to find a quadratic δ_3 -ISS Lyapunov function for system Σ_η in (4.10).

Remark 4.8. It can be verified that the backstepping design approach for strict-feedback form control systems, proposed in [3], is a special case of the results in [Lemma 4.6](#). The results in [3] can

be easily obtained by recursively applying the results proposed in [Lemma 4.6](#). Moreover, one can construct a metric \mathbf{d} for a strict-feedback form control system, satisfying (2.1) or (2.2), by recursively applying the construction in (4.11) and applying the change of coordinate in (4.7).

The next lemma shows how to construct contraction metrics for the closed-loop system resulting from the backstepping controller synthesis technique in [Theorem 4.2](#).

Lemma 4.9. Consider the control system Σ of the form (4.1) and assume function f is smooth. Suppose there exists a continuously differentiable function $\psi : \mathbb{R}^{n_\eta} \rightarrow \mathbb{R}^{n_\zeta}$ such that the metric $\hat{G} : \mathbb{R}^{n_\eta} \rightarrow \mathbb{R}^{n_\eta \times n_\eta}$ is a contraction metric, with respect to states and inputs, for the control system

$$\Sigma_\eta : \dot{\eta} = f(\eta, \psi(\eta) + \tilde{v}),$$

satisfying the condition (3.21) for some $\hat{\lambda} \in \mathbb{R}^+$ and $\alpha \in \mathbb{R}_0^+$. Then

$$\tilde{G}(x) = \begin{bmatrix} \hat{G}(y) + \left(\frac{\partial \psi}{\partial y} \right)^T \frac{\partial \psi}{\partial y} & - \left(\frac{\partial \psi}{\partial y} \right)^T \\ - \frac{\partial \psi}{\partial y} & I_{n_\zeta} \end{bmatrix},$$

where $x = [y^T, z^T]^T$, is a contraction metric, with respect to states and inputs, for Σ as in (4.1) equipped with the state feedback control law in (4.6) for all $\lambda > \frac{\alpha^2}{8\hat{\lambda}}$.

Proof. As explained in the proof of [Theorem 4.2](#), using the proposed control law (4.6) and the coordinate transformation ϕ in (4.7), the control system Σ of the form (4.1) is transformed to the control system $\tilde{\Sigma}$ in (4.9). Now we show that the metric

$$G(\hat{x}) = \begin{bmatrix} \hat{G}(\hat{x}_1) & 0_{n_\eta \times n_\zeta} \\ 0_{n_\zeta \times n_\eta} & I_{n_\zeta} \end{bmatrix},$$

is a contraction metric, with respect to states and inputs, for $\tilde{\Sigma}$, where $\hat{x} = [\hat{x}_1^T, \hat{x}_2^T]^T$ is the state of $\tilde{\Sigma}$, and \hat{x}_1 , and \hat{x}_2 are states of χ_1, χ_2 -subsystems, respectively. It can be easily seen that G is positive definite because \hat{G} is positive definite since it is a contraction metric for Σ_η . Now we show that G satisfies the condition (3.21) for the control system $\tilde{\Sigma}$. Since \hat{G} is a contraction metric, with respect to states and inputs, for χ_1 -subsystem when χ_2 is the input, we have:

$$\begin{aligned} & \hat{x}_1^T \left(\left(\frac{\partial f}{\partial \hat{x}_1} \right)^T \hat{G}(\hat{x}_1) + \hat{G}(\hat{x}_1) \frac{\partial f}{\partial \hat{x}_1} \right. \\ & \quad \left. + \frac{\partial \hat{G}}{\partial \hat{x}_1} f(\hat{x}_1, \psi(\hat{x}_1) + \hat{x}_2) \right) \hat{x}_1 + 2\hat{x}_2^T \left(\frac{\partial f}{\partial \hat{x}_2} \right)^T \hat{G}(\hat{x}_1) \hat{x}_1 \\ & \leq -\hat{\lambda} \hat{x}_1^T \hat{G}(\hat{x}_1) \hat{x}_1 + \alpha (\hat{x}_1^T \hat{G}(\hat{x}_1) \hat{x}_1)^{\frac{1}{2}} (\hat{x}_2^T \hat{x}_2)^{\frac{1}{2}}, \end{aligned} \quad (4.12)$$

for any $\hat{x}_1, \hat{x}'_1 \in \mathbb{R}^{n_\eta}$, $\hat{x}_2, \hat{x}'_2 \in \mathbb{R}^{n_\zeta}$, some $\hat{\lambda} \in \mathbb{R}^+$, and some $\alpha \in \mathbb{R}_0^+$. By choosing $\lambda > \frac{\alpha^2}{8\hat{\lambda}}$, using (4.12), and the Cauchy Schwarz inequality we obtain the chain of inequalities in (4.13) for any $\hat{x} = [\hat{x}_1^T, \hat{x}_2^T]^T \in \mathbb{R}^{n_\eta+n_\zeta}$, any $\hat{x}' = [\hat{x}'_1^T, \hat{x}'_2^T]^T \in \mathbb{R}^{n_\eta+n_\zeta}$, any $Y \in \mathbb{R}^{n_\zeta}$, and some $\hat{\lambda} \in \mathbb{R}^+$.

$$\begin{aligned} & [\hat{x}_1^T, \hat{x}_2^T] \cdot \left(\left(\frac{\partial [f, -\lambda \hat{x}_2 + \hat{u}]^T}{\partial \hat{x}} \right)^T G(\hat{x}) \right. \\ & \quad \left. + G(\hat{x}) \frac{\partial [f, -\lambda \hat{x}_2 + \hat{u}]^T}{\partial \hat{x}} + \frac{\partial G}{\partial \hat{x}} \begin{bmatrix} f(\hat{x}_1, \psi(\hat{x}_1) + \hat{x}_2) \\ -\lambda \hat{x}_2 + \hat{u} \end{bmatrix} \right) \end{aligned}$$

$$\begin{aligned}
& \cdot \begin{bmatrix} \widehat{X}_1 \\ \widehat{X}_2 \end{bmatrix} + 2Y^T \begin{bmatrix} 0_{n_\eta \times n_\zeta} \\ I_{n_\zeta} \end{bmatrix}^T G(\widehat{X}) \begin{bmatrix} \widehat{X}_1 \\ \widehat{X}_2 \end{bmatrix} = [\widehat{X}_1^T \widehat{X}_2^T] \\
& \cdot \begin{bmatrix} \left(\frac{\partial f}{\partial \widehat{X}_1} \right)^T \widehat{G}(\widehat{x}_1) + \widehat{G}(\widehat{x}_1) \frac{\partial f}{\partial \widehat{X}_1} + \frac{\partial \widehat{G}}{\partial \widehat{X}_1} f & \widehat{G}(\widehat{x}_1) \frac{\partial f}{\partial \widehat{X}_2} \\ \left(\frac{\partial f}{\partial \widehat{X}_2} \right)^T \widehat{G}(\widehat{x}_1) & -2\lambda I_{n_\zeta} \end{bmatrix} \\
& \cdot \begin{bmatrix} \widehat{X}_1 \\ \widehat{X}_2 \end{bmatrix} + 2Y^T \widehat{X}_2 \leq -\widehat{\lambda} \langle \widehat{X}_1, \widehat{X}_1 \rangle_{\widehat{G}} \\
& + \alpha \langle \widehat{X}_1, \widehat{X}_1 \rangle_{\widehat{G}}^{\frac{1}{2}} \langle \widehat{X}_2, \widehat{X}_2 \rangle_{I_{n_\zeta}}^{\frac{1}{2}} - 2\lambda \widehat{X}_2^T \widehat{X}_2 + 2Y^T \widehat{X}_2 \\
& \leq -\widehat{\lambda} \langle \widehat{X}_1, \widehat{X}_1 \rangle_{\widehat{G}} - \widetilde{\lambda} \widehat{X}_2^T \widehat{X}_2 \\
& + 2\sqrt{Y^T Y} \sqrt{\widehat{X}_2^T \widehat{X}_2} + \langle \widehat{X}_1, \widehat{X}_1 \rangle_{\widehat{G}} \\
& \leq -\widetilde{\lambda} \langle \widehat{X}, \widehat{X} \rangle_{\widehat{G}} + 2 \langle \widehat{X}, \widehat{X} \rangle_{\widehat{G}}^{\frac{1}{2}} \langle Y, Y \rangle^{\frac{1}{2}}. \quad (4.13)
\end{aligned}$$

Hence, G is a contraction metric, with respect to states and inputs, for $\widehat{\Sigma}$. Since a contraction metric, with respect to states and inputs, is coordinate invariant [2], we conclude that $\widehat{G} = \phi^* G$ is a contraction metric, with respect to states and inputs, for Σ as in (4.1) equipped with the state feedback control law in (4.6). This completes the proof.

Remark 4.10. It can be verified that the backstepping design approach for strict-feedback form control systems, proposed in [2], is a special case of the results in Lemma 4.9. The results in [2] can be easily obtained by recursively applying the results proposed in Lemma 4.9.

5. Example

We illustrate the results of this paper on two different examples. Both examples are unstable non-smooth control systems that does not satisfy the assumptions required in [19–21,2,3]. The results in [15] also cannot be applied here because they would result in a closed-loop system which is input-to-state convergent rather than δ_3 -ISS. The first example involves a four-dimensional control system and aims to show how to recursively construct a δ_3 -ISS Lyapunov function. The second example involves a two-dimensional non-smooth control system and aims at elucidating the role of incremental Lyapunov functions in enabling the construction of finite abstractions of nonlinear control systems. The reader interested in additional examples can also consult [42] for a physical example on a synchronous generator to which the results proposed in Lemmas 4.6 and 4.9 can be applied recursively.

5.1. Example 1

The example in this section illustrates the application of the results in the paper to design controllers rendering a system incrementally stable and to recursively construct a δ_3 -ISS Lyapunov function. Consider the following non-smooth control system:

$$\Sigma : \begin{cases} \dot{\eta}_1 = -\eta_1 + |\eta_3|, \\ \dot{\eta}_2 = -\eta_2 + \text{sat}(\eta_1) \text{sat}(\eta_3), \\ \dot{\eta}_3 = \eta_3 + \eta_1 \eta_2 \eta_3 + \eta_3^3 + \zeta_1, \\ \dot{\zeta}_1 = \zeta_1 + \zeta_1^3 + \eta_3^2 + \nu, \end{cases} \quad (5.1)$$

where $\text{sat} : \mathbb{R} \rightarrow \mathbb{R}$ is the saturation function, defined by:

$$\text{sat}(x) = \begin{cases} -1 & \text{if } x < -1, \\ x & \text{if } |x| \leq 1, \\ 1 & \text{if } x > 1. \end{cases} \quad (5.2)$$

It can be readily verified that for $\nu(t) = 0$ for any $t \in \mathbb{R}_0^+$, Σ is unstable at $(0, 0, 0, 0)$, implying that Σ is not δ_3 -ISS. By introducing the feedback transformation $\widehat{\nu} = \zeta_1 + \zeta_1^3 + \eta_3^2 + \nu$, the control system Σ is transformed into:

$$\widehat{\Sigma} : \begin{cases} \dot{\eta}_1 = -\eta_1 + |\eta_3|, \\ \dot{\eta}_2 = -\eta_2 + \text{sat}(\eta_1) \text{sat}(\eta_3), \\ \dot{\eta}_3 = \eta_3 + \eta_1 \eta_2 \eta_3 + \eta_3^3 + \zeta_1, \\ \dot{\zeta}_1 = \widehat{\nu}. \end{cases}$$

Now by choosing $\psi(\eta) = -4\eta_3 - \eta_1 \eta_2 \eta_3 - \eta_3^3$ and substituting $\psi(\eta) + \widehat{\nu}$ instead of ζ_1 , we obtain the following η -subsystem:

$$\widehat{\Sigma}_\eta : \begin{cases} \dot{\eta}_1 = -\eta_1 + |\eta_3|, \\ \dot{\eta}_2 = -\eta_2 + \text{sat}(\eta_1) \text{sat}(\eta_3), \\ \dot{\eta}_3 = \eta_3 + \eta_1 \eta_2 \eta_3 + \eta_3^3 + \psi(\eta) + \widehat{\nu} = -3\eta_3 + \widehat{\nu}. \end{cases}$$

It remains to show that $\widehat{\Sigma}_\eta$ is δ_3 -ISS with respect to $\widehat{\nu}$. We will do so in a recursive fashion. First we show that the control system:

$$\widehat{\Sigma}_1 : \dot{\eta}_1 = -\eta_1 + |\eta_3|, \quad (5.3)$$

is δ_3 -ISS with respect to the input η_3 . By choosing the function $V_1(y_1, y'_1) = (y_1 - y'_1)^2$, where y_1 and y'_1 are states of $\widehat{\Sigma}_1$, and using the Cauchy Schwarz inequality, we have that:

$$\begin{aligned}
& \frac{\partial V_1}{\partial y_1} (-y_1 + |y_3|) + \frac{\partial V_1}{\partial y'_1} (-y'_1 + |y'_3|) \\
& \leq -2(y_1 - y'_1)^2 + 2|y_1 - y'_1| |y_3 - y'_3| \\
& \leq -V_1(y_1, y'_1) + |y_3 - y'_3|^2,
\end{aligned}$$

showing that V_1 is a δ_3 -ISS Lyapunov function for $\widehat{\Sigma}_1$ in (5.3) and, hence, $\widehat{\Sigma}_1$ is δ_3 -ISS with respect to the input η_3 . Second, we show that the control system:

$$\widehat{\Sigma}_2 : \dot{\eta}_2 = -\eta_2 + \text{sat}(\eta_1) \text{sat}(\eta_3), \quad (5.4)$$

is δ_3 -ISS with respect to inputs η_1 and η_3 . Similarly, it can be shown that the function $V_2(y_2, y'_2) = (y_2 - y'_2)^2$, where y_2 and y'_2 are states of $\widehat{\Sigma}_2$, is a δ_3 -ISS Lyapunov function for $\widehat{\Sigma}_2$ in (5.4). Hence, $\widehat{\Sigma}_2$ is δ_3 -ISS with respect to inputs η_1 and η_3 . Third, it can be shown in a similar fashion that the control system:

$$\widehat{\Sigma}_3 : \dot{\eta}_3 = -3\eta_3 + \widehat{\nu},$$

is δ_3 -ISS with respect to the input $\widehat{\nu}$. By virtue of Lemma 4.1, we conclude that the control system $\widehat{\Sigma}_\eta$ is δ_3 -ISS with respect to $\widehat{\nu}$. By using the results in Theorem 4.2 for the control system $\widehat{\Sigma}$, we conclude that the state feedback control law:

$$\begin{aligned}
\widehat{\nu} &= k(\eta, \zeta, \bar{\nu}) = -\lambda(\zeta_1 - \psi(\eta)) + \frac{\partial \psi}{\partial y} \dot{\eta} + \bar{\nu} \\
&= -\lambda(\zeta_1 + 4\eta_3 + \eta_1 \eta_2 \eta_3 + \eta_3^3) \\
&\quad + (\eta_3 + \eta_1 \eta_2 \eta_3 + \eta_3^3 + \zeta_1) (-4 - \eta_1 \eta_2 - 3\eta_3^2) \\
&\quad - \eta_2 \eta_3 (-\eta_1 + |\eta_3|) - \eta_1 \eta_3 \\
&\quad \times (-\eta_2 + \text{sat}(\eta_1) \text{sat}(\eta_3)) + \bar{\nu}, \quad (5.5)
\end{aligned}$$

renders the control system $\widehat{\Sigma}$ δ_3 -ISS with respect to input $\bar{\nu}$, for any $\lambda \in \mathbb{R}^+$. Therefore, the state feedback control law

$$\nu = \widehat{k}(\eta, \zeta, \bar{\nu}) = k(\eta, \zeta, \bar{\nu}) - \zeta_1 - \zeta_1^3 - \eta_3^2, \quad (5.6)$$

renders the control system Σ δ_3 -ISS with respect to input $\bar{\nu}$.

Let us now aim for finding a δ_3 -ISS Lyapunov function $V : \mathbb{R}^4 \times \mathbb{R}^4 \rightarrow \mathbb{R}_0^+$ for the control system Σ in (5.1), equipped with the state feedback control law \widehat{k} in (5.6). It can be shown that the function $\widehat{V}(y, y') = (y_1 - y'_1)^2 + (y_2 - y'_2)^2 + (y_3 - y'_3)^2$ is a δ_3 -ISS

Lyapunov function for the control system $\widehat{\Sigma}_\eta$. Using Theorem 4.6, we conclude that the function:

$$\begin{aligned} V(x, x') &= \widehat{V}(y, y') + |(z_1 - \psi(y)) - (z'_1 - \psi(y'))|^2 \\ &= (y_1 - y'_1)^2 + (y_2 - y'_2)^2 + (y_3 - y'_3)^2 \\ &\quad + ((z_1 + 4y_3 + y_1 y_2 y_3 + y_3^3) \\ &\quad - (z'_1 + 4y'_3 + y'_1 y'_2 y'_3 + y'^3_3))^2, \end{aligned} \quad (5.7)$$

where $x = [y_1, y_2, y_3, z_1]^T$ is the state of Σ , is a δ_3 -ISS Lyapunov function for the control system Σ equipped with the state feedback control law \widehat{k} in (5.6) with $\lambda > \frac{5}{4}$.

We simulate the closed-loop system with $\lambda = 5$ and $\bar{v}(t) = 10 \sin(2t)$, for any $t \in \mathbb{R}_0^+$. In Fig. 1, we show the closed-loop trajectories stemming from the initial conditions $(1, 1, 1, 1)$ and $(-1, -1, -1, -1)$, respectively. The figure shows that indeed, by virtue of the δ_3 -ISS property, both trajectories converge to each other.

5.2. Example 2

Consider the following non-smooth control system:

$$\Sigma : \begin{cases} \dot{\eta}_1 = \text{sat}(\eta_1) + \eta_1 + 5\zeta_1, \\ \dot{\zeta}_1 = \zeta_1^2 + \eta_1^2 + v, \end{cases} \quad (5.8)$$

where $\text{sat} : \mathbb{R} \rightarrow \mathbb{R}$ is the saturation function, defined in (5.2).

It can be readily verified that Σ is unstable at $(0, 0)$, implying that Σ is not δ_3 -ISS. Note that here we require δ_3 -ISS and a δ_3 -ISS Lyapunov function in order to construct a finite equivalent abstraction using the results in [11]. By introducing the feedback transformation $\widehat{v} = \zeta_1^2 + \eta_1^2 + v$, the control system Σ is transformed into the following form:

$$\widehat{\Sigma} : \begin{cases} \dot{\eta}_1 = \text{sat}(\eta_1) + \eta_1 + 5\zeta_1, \\ \dot{\zeta}_1 = \widehat{v}. \end{cases}$$

Now by choosing $\psi(\eta_1) = -\eta_1$ and substituting $\psi(\eta_1) + \widehat{v}$ instead of ζ_1 , we obtain the following η -subsystem:

$$\widehat{\Sigma}_\eta : \dot{\eta}_1 = \text{sat}(\eta_1) + \eta_1 + 5(\psi(\eta_1) + \widehat{v}) = \text{sat}(\eta_1) - 4\eta_1 + 5\widehat{v}.$$

It remains to show that $\widehat{\Sigma}_\eta$ is δ_3 -ISS with respect to \widehat{v} . By choosing the function $V_1(y_1, y'_1) = (y_1 - y'_1)^2$, where y_1 and y'_1 are states of $\widehat{\Sigma}_\eta$, and using the Cauchy Schwarz inequality, we have that:

$$\begin{aligned} \frac{\partial V_1}{\partial y_1} (\text{sat}(y_1) - 4y_1 + 5\widehat{v}) + \frac{\partial V_1}{\partial y'_1} (\text{sat}(y'_1) - 4y'_1 + 5\widehat{v}') \\ \leq -8(y_1 - y'_1)^2 + 2|y_1 - y'_1| |\text{sat}(y_1) - \text{sat}(y'_1)| \\ + 10(y_1 - y'_1)(\widehat{v} - \widehat{v}') \leq -8(y_1 - y'_1)^2 + 2(y_1 - y'_1)^2 \\ + 10(y_1 - y'_1)(\widehat{v} - \widehat{v}') \leq -5(y_1 - y'_1)^2 + 25(\widehat{v} - \widehat{v}')^2, \end{aligned}$$

showing that V_1 is a δ_3 -ISS Lyapunov function for $\widehat{\Sigma}_\eta$ and, hence, $\widehat{\Sigma}_\eta$ is δ_3 -ISS with respect to \widehat{v} . By using the results in Theorem 4.2 for the control system $\widehat{\Sigma}$, we conclude that the state feedback control law:

$$\begin{aligned} \widehat{v} &= k(\eta_1, \zeta_1, \bar{v}) = -\lambda(\zeta_1 - \psi(\eta_1)) + \frac{\partial \psi}{\partial y_1} \dot{\eta}_1 + \bar{v} \\ &= -\lambda(\zeta_1 + \eta_1) - (\text{sat}(\eta_1) + \eta_1 + 5\zeta_1) + \bar{v}, \end{aligned}$$

renders the control system $\widehat{\Sigma}_{\delta_3}$ -ISS with respect to input \bar{v} , for any $\lambda \in \mathbb{R}^+$. Therefore, the state feedback control law

$$v = \widehat{k}(\eta_1, \zeta_1, \bar{v}) = k(\eta_1, \zeta_1, \bar{v}) - \eta_1^2 - \zeta_1^2, \quad (5.9)$$

makes the control system Σ_{δ_3} -ISS with respect to input \bar{v} .

Using Lemma 4.6, we conclude that the function $V : \mathbb{R}^2 \times \mathbb{R}^2 \rightarrow \mathbb{R}_0^+$, defined by:

$$\begin{aligned} V(x, x') &= V_1(y_1, y'_1) + |(z_1 - \psi(y_1)) - (z'_1 - \psi(y'_1))|^2 \\ &= (y_1 - y'_1)^2 + ((z_1 + y_1) - (z'_1 + y'_1))^2 \\ &= (x - x')^T P (x - x') \\ &= (x - x')^T \begin{bmatrix} 2 & 1 \\ 1 & 1 \end{bmatrix} (x - x'), \end{aligned}$$

where $x = [y_1, z_1]^T$ is the state of Σ , is a δ_3 -ISS Lyapunov function for the control system Σ equipped with the state feedback control law \widehat{k} in (5.9) with $\lambda > \frac{25+5+1}{2}$. Here, we choose $\lambda = 16$.

It can be readily verified that the function $\widehat{V}(x, x') = \sqrt{V(x, x')}$ is also a δ_3 -ISS Lyapunov function for the control system Σ equipped with the state feedback control law \widehat{k} in (5.9) with $\lambda > \frac{25+5+1}{2}$, satisfying:

- (i) for any $x, x' \in \mathbb{R}^2$, $\sqrt{\lambda_{\min}(P)} \|x - x'\| \leq \widehat{V}(x, x') \leq \sqrt{\lambda_{\max}(P)} \|x - x'\|$;
- (ii) for any $x, x' \in \mathbb{R}^2$ and for any $\bar{u}, \bar{u}' \in \bar{U} \subseteq \mathbb{R}$, $\frac{\partial \widehat{V}}{\partial x} f(x, \widehat{k}(x, \bar{u})) + \frac{\partial \widehat{V}}{\partial x'} f(x', \widehat{k}(x', \bar{u}')) \leq -2.5\widehat{V}(x, x') + \frac{|\bar{u} - \bar{u}'|}{\lambda_{\min}(P)}$;
- (iii) for any $x, y, z \in \mathbb{R}^2$, $|\widehat{V}(x, y) - \widehat{V}(x, z)| \leq \frac{\lambda_{\max}(P)}{\sqrt{\lambda_{\min}(P)}} \|y - z\|$;

where $\lambda_{\min}(P)$, and $\lambda_{\max}(P)$ indicate, respectively, the minimum and maximum eigenvalues of P . Note that, the property (iii) is a consequence of Proposition 10.5 in [29].

Finite abstractions are simpler descriptions of control systems, with finitely many states, in which each state of the abstraction represents a collection or aggregate of states in the control system. Similar finite abstractions are used in software and hardware modeling, which enables the composition of such (hardware/software) abstractions with the finite abstraction of the control system. The result of this composition are finite abstractions capturing the behavior of the control system interacting with the digital computational devices. Once such abstractions are available, the methodologies and tools developed in computer science for verification and controller synthesis purposes can be easily employed to control systems, via these abstractions. However, for constructing a bisimilar finite abstraction, using the results in [11] which does not impose any restriction on the sampling time, the control system is required to be incrementally stable and to exhibit an incremental Lyapunov function. The incremental stability property bounds the error propagations coming from discretization of the state space and input set in the process of constructing the finite bisimilar abstractions. We refer the interested readers to [29] for more detailed information about the finite abstractions and their great advantages in controller synthesis problems.

Now, we construct a finite abstraction $S(\Sigma)$ for the control system Σ , equipped with the control input v in (5.9), using the results in [11]. We assume that $\bar{v}(t) \in \bar{U} = [-10, 10]$, for any $t \in \mathbb{R}_0^+$, and \bar{v} belongs to set \bar{U} that contains piecewise constant curves of duration $\tau = 0.1$ second (τ is the sampling time) taking values in $[\bar{U}]_{0.5} = \{\bar{u} \in \bar{U} \mid \bar{u} = 0.5k, k \in \mathbb{Z}\}$. We work on the subset $D = [-1, 1] \times [-1, 1]$ of the state space Σ . For a given precision¹² $\varepsilon = 0.1$ and using properties (i)–(iii) of \widehat{V} , we conclude that D should be quantized with resolution of $\eta = 0.009$, using the results of Theorem 4.1 in [11]. The state set of $S(\Sigma)$ is $[D]_\eta = \{x \in D \mid x_i = k_i \eta, k_i \in \mathbb{Z}, i = 1, 2\}$. It can be readily seen that the set $[D]_\eta$ is finite. The computation of the finite

¹² The parameter ε is the maximum error between a trajectory of the control system and its corresponding trajectory from the finite abstraction at times $k\tau$, $k \in \mathbb{N}_0$, with respect to the Euclidean metric.

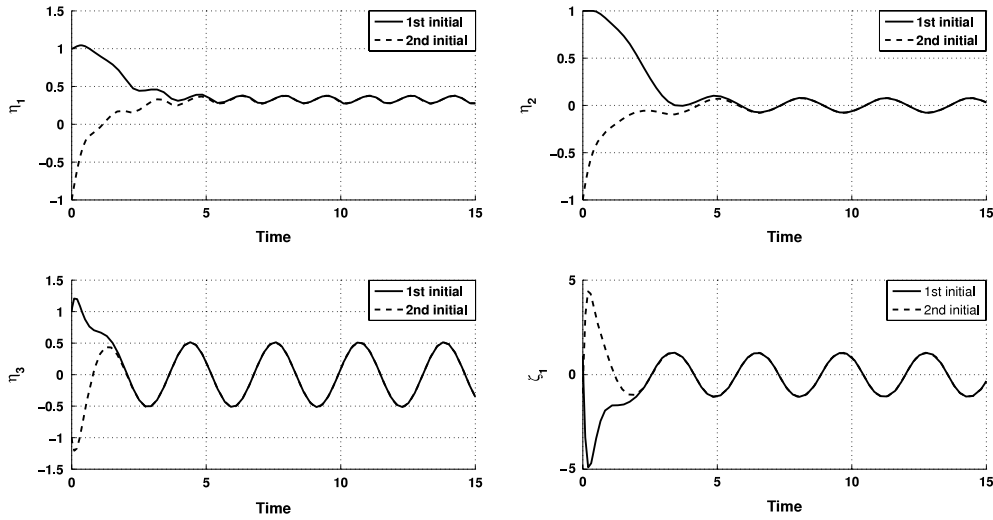


Fig. 1. Evolution of η_1 , η_2 , η_3 , and ζ_1 with the input $\bar{v}(t) = 10 \sin(2t)$ and initial conditions $(1, 1, 1, 1)$, and $(-1, -1, -1, -1)$, respectively.

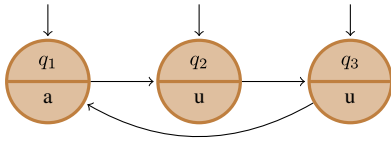


Fig. 2. Finite system describing the schedulability constraints. The lower part of the states are labeled with the outputs a and u denoting availability and unavailability of the microprocessor, respectively.

abstraction $S(\Sigma)$ was performed using the tool Pessoa [43]. Using the computed finite abstraction, we can synthesize controllers, providing \bar{v} in (5.9), satisfying specifications that are difficult to enforce with conventional controller design methods. Here, our objective is to design a controller navigating the trajectories of Σ , equipped with the control input v in (5.9), to reach the target set $W = [-0.05, 0.05] \times [-0.05, 0.05]$, indicated with a red box in Fig. 3, while avoiding the obstacles, indicated as blue boxes in Fig. 3, and remain indefinitely inside W . Furthermore, we assume that the controller is implemented on a microprocessor, which is executing other tasks in addition to the control task. We consider a schedule with epochs of three time slots in which the first slot is allocated to the control task and the other two to other tasks. A time slot refers to a time interval of the form $[k\tau, (k+1)\tau]$ with $k \in \mathbb{N}$ and where τ is the sampling time. Therefore, the microprocessor schedules is given by (depending on the initial slot):

$|auu|auu|auu|auu|auu|auu|auu| \dots$,
 $|uuu|uuu|uuu|uuu|uuu|uuu|uuu| \dots$,
 $|uau|uau|uau|uau|uau|uau|uau| \dots$,

where a denotes a slot available for the control task and u denotes a slot allotted to other tasks. We assume that in unallocated time slots, the input \bar{v} is identically zero. The schedulability constraint on the microprocessor can be represented by the finite system in Fig. 2.

A controller, providing \bar{v} in (5.9) and enforcing the specification has been designed by using standard algorithms from game theory, implemented in Pessoa, where the finite system is initialized from state q_2 , see second sequence above. In Fig. 3, we show the closed-loop trajectories of Σ , equipped with the control input v in (5.9) (including the additional controller for \bar{v}) and stemming from the initial conditions $[0.8, 0.9]$ and $[-0.8, -0.9]$. It is readily seen that the specifications are satisfied. In Fig. 4, we show the evolution of the input signal \bar{v} in (5.9) corresponding to the two initial

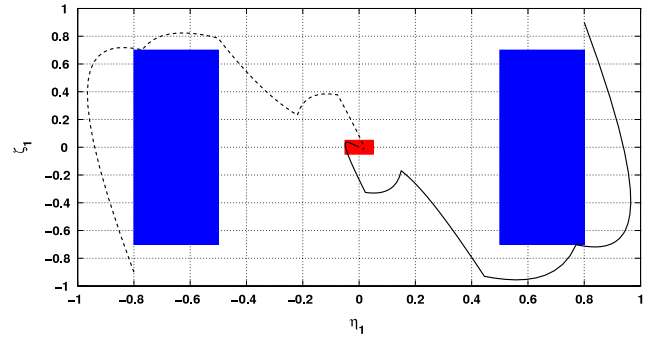


Fig. 3. Evolutions of the closed-loop system with initial conditions $(0.8, 0.9)$, and $(-0.8, -0.9)$.

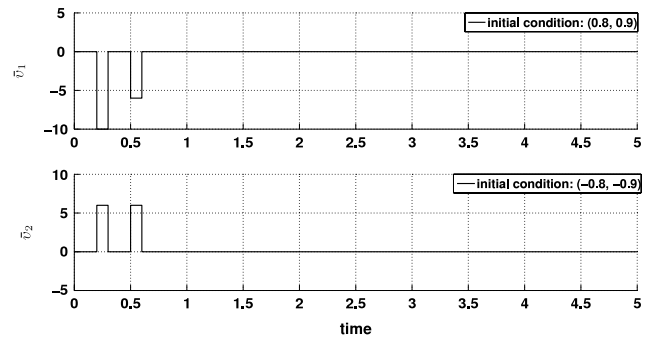


Fig. 4. Evolutions of the input signals \bar{v}_1 and \bar{v}_2 , corresponding to initial conditions $(0.8, 0.9)$, and $(-0.8, -0.9)$, respectively.

conditions. It can be easily seen that the schedulability constraint is also satisfied, implying that the control input \bar{v} is identically zero at unallocated time slots.

Resuming, we employed the results in this paper to render the closed-loop system incrementally stable and to construct an incremental Lyapunov function for the closed-loop system. The explicit availability of an incremental Lyapunov function allowed us to use the results in [11] to construct a finite abstraction $S(\Sigma)$ for the control system Σ in (5.8), equipped with the control input in (5.9). This finite abstraction allowed us to use tools developed in computer since to synthesize a controller satisfying some logic specifications difficult to enforce using conventional controller synthesis methods.

6. Discussion

In this paper we provided the characterizations of incremental stability, defined in [2], in terms of existence of incremental Lyapunov functions, defined in [3]. We also provided sufficient conditions for incremental stability in terms of contraction metrics. Moreover, we developed a backstepping procedure to design controllers enforcing incremental input-to-state stability (or contraction properties) for the resulting closed-loop system. The proposed approach in this paper generalizes the work in [19–21,2,3] by being applicable to larger classes of control systems and the work in [15] by enforcing incremental input-to-state stability rather than input-to-state convergence. Moreover, in contrast to the proposed backstepping design approach in [15], here we provided a way of constructing incremental Lyapunov functions, which are known to be a key tool in the analysis provided in [11, 24,26,28]. As we showed in one of the examples in the paper, the explicit existence of an incremental Lyapunov function helps us to use the results in [11] to construct a finite bisimilar abstraction for a resulting incrementally stable closed-loop (non-smooth) control system.

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Appendix

Proof of Lemma 4.1. The proof was inspired by the proof of Proposition 4.7 in [1]. The essential differences lie in the choice of the metric for the overall system Σ using the metrics for η , ζ -subsystems. We provide the proof so that it can be easily compared with the proof in [1]. Using (4.3), (4.4) and triangle inequality, the chain of inequalities in (A.1) hold, where $\hat{\gamma} \in \mathcal{K}_\infty$ and $\hat{\beta}, \tilde{\beta} \in \mathcal{K}\mathcal{L}$ in (A.1) are defined as following:

$$\begin{aligned} \hat{\gamma}(r) &= \beta_\eta(3\gamma_\zeta(2\tilde{\gamma}_v(r)), 0) + \beta_\eta(3\gamma_v(r), 0) \\ &\quad + \gamma_\zeta(2\tilde{\gamma}_v(r)) + \gamma_v(r), \\ \hat{\beta}(r, t) &= \beta_\eta(3\beta_\eta(r, t/2), t/2), \\ \tilde{\beta}(r, t) &= \beta_\eta(3\gamma_\zeta(2\beta_\zeta(r, 0)), t/2) + \gamma_\zeta(2\beta_\zeta(r, t/2)) \\ \mathbf{d}_\eta(\eta_{y\zeta v}(t), \eta_{y'\zeta'v'}(t)) \\ &\leq \beta_\eta(\mathbf{d}_\eta(\eta_{y\zeta v}(t/2), \eta_{y'\zeta'v'}(t/2)), t/2) \\ &\quad + \gamma_\zeta(\mathbf{d}_\zeta(\zeta, \zeta')_{[t/2, \infty)}) + \gamma_v(\|v - v'\|_{[t/2, \infty)}) \\ &\leq \beta_\eta(\beta_\eta(\mathbf{d}_\eta(y, y'), t/2) \\ &\quad + \gamma_\zeta(\mathbf{d}_\zeta(\zeta, \zeta')_\infty) + \gamma_v(\|v - v'\|_\infty), t/2) \\ &\quad + \gamma_\zeta(\mathbf{d}_\zeta(\zeta, \zeta')_{[t/2, \infty)}) + \gamma_v(\|v - v'\|_{[t/2, \infty)}) \\ &\leq \beta_\eta(3\beta_\eta(\mathbf{d}_\eta(y, y'), t/2), t/2) \\ &\quad + \beta_\eta(3\gamma_\zeta(\mathbf{d}_\zeta(\zeta, \zeta')_\infty), t/2) \\ &\quad + \beta_\eta(3\gamma_v(\|v - v'\|_\infty), 0) \\ &\quad + \gamma_\zeta(\mathbf{d}_\zeta(\zeta, \zeta')_{[t/2, \infty)}) + \gamma_v(\|v - v'\|_{[t/2, \infty)}) \\ &\leq \beta_\eta(3\beta_\eta(\mathbf{d}_\eta(y, y'), t/2), t/2) \\ &\quad + \beta_\eta(3\gamma_\zeta(\beta_\zeta(\mathbf{d}_\zeta(z, z'), 0) + \tilde{\gamma}_v(\|v - v'\|_\infty)), t/2) \\ &\quad + \beta_\eta(3\gamma_v(\|v - v'\|_\infty), 0) + \gamma_\zeta(\mathbf{d}_\zeta(\zeta, \zeta')_{[t/2, \infty)}) \\ &\quad + \gamma_v(\|v - v'\|_{[t/2, \infty)}) \end{aligned}$$

$$\begin{aligned} &\leq \beta_\eta(3\beta_\eta(\mathbf{d}_\eta(y, y'), t/2), t/2) \\ &\quad + \beta_\eta(3\gamma_\zeta(2\beta_\zeta(\mathbf{d}_\zeta(z, z'), 0)), t/2) \\ &\quad + \beta_\eta(3\gamma_\zeta(2\tilde{\gamma}_v(\|v - v'\|_\infty)), t/2) \\ &\quad + \beta_\eta(3\gamma_v(\|v - v'\|_\infty), 0) \\ &\quad + \gamma_\zeta(\mathbf{d}_\zeta(\zeta, \zeta')_{[t/2, \infty)}) + \gamma_v(\|v - v'\|_{[t/2, \infty)}) \\ &\leq \beta_\eta(3\beta_\eta(\mathbf{d}_\eta(y, y'), t/2), t/2) \\ &\quad + \beta_\eta(3\gamma_\zeta(2\beta_\zeta(\mathbf{d}_\zeta(z, z'), 0)), t/2) \\ &\quad + \beta_\eta(3\gamma_\zeta(2\tilde{\gamma}_v(\|v - v'\|_\infty)), 0) \\ &\quad + \beta_\eta(3\gamma_v(\|v - v'\|_\infty), 0) \\ &\quad + \gamma_\zeta(\beta_\zeta(\mathbf{d}_\zeta(z, z'), t/2) \\ &\quad + \tilde{\gamma}_v(\|v - v'\|_\infty)) + \gamma_v(\|v - v'\|_{[t/2, \infty)}) \\ &\leq \beta_\eta(3\beta_\eta(\mathbf{d}_\eta(y, y'), t/2), t/2) \\ &\quad + \beta_\eta(3\gamma_\zeta(2\beta_\zeta(\mathbf{d}_\zeta(z, z'), 0)), t/2) \\ &\quad + \beta_\eta(3\gamma_\zeta(2\tilde{\gamma}_v(\|v - v'\|_\infty)), 0) \\ &\quad + \beta_\eta(3\gamma_v(\|v - v'\|_\infty), 0) \\ &\quad + \gamma_\zeta(2\beta_\zeta(\mathbf{d}_\zeta(z, z'), t/2) + \gamma_\zeta(2\tilde{\gamma}_v(\|v - v'\|_\infty)) \\ &\quad + \gamma_v(\|v - v'\|_\infty)) \\ &\leq \hat{\beta}(\mathbf{d}_\eta(y, y'), t) + \tilde{\beta}(\mathbf{d}_\zeta(z, z'), t) + \hat{\gamma}(\|v - v'\|_\infty). \quad (\text{A.1}) \end{aligned}$$

Now we define a new metric $\mathbf{d} : \mathbb{R}^{n_\eta+n_\zeta} \times \mathbb{R}^{n_\eta+n_\zeta} \rightarrow \mathbb{R}_0^+$ by:

$$\mathbf{d}(x, x') = \mathbf{d}_\eta(y, y') + \mathbf{d}_\zeta(z, z'), \quad (\text{A.2})$$

for any $x = [y^T, z^T]^T \in \mathbb{R}^{n_\eta+n_\zeta}$ and $x' = [y'^T, z'^T]^T \in \mathbb{R}^{n_\eta+n_\zeta}$. It can be readily checked that \mathbf{d} satisfies all three conditions of a metric. By defining $\xi_{xv} = [\eta_{y\zeta v}^T, \zeta_{zv}^T]^T$, using inequalities (4.4) and (A.1), and for any $t \in \mathbb{R}_0^+$, any $x, x' \in \mathbb{R}^{n_\eta+n_\zeta}$, and any $v, v' \in \mathcal{U}$, we obtain:

$$\begin{aligned} \mathbf{d}(\xi_{xv}(t), \xi_{x'v'}(t)) \\ &= \mathbf{d}_\eta(\eta_{y\zeta v}(t), \eta_{y'\zeta'v'}(t)) + \mathbf{d}_\zeta(\zeta_{zv}(t), \zeta_{z'v'}(t)) \\ &\leq \hat{\beta}(\mathbf{d}_\eta(y, y'), t) + \tilde{\beta}(\mathbf{d}_\zeta(z, z'), t) + \hat{\gamma}(\|v - v'\|_\infty) \\ &\quad + \beta_\zeta(\mathbf{d}_\zeta(z, z'), t) + \tilde{\gamma}_v(\|v - v'\|_\infty) \\ &\leq \hat{\beta}(\mathbf{d}_\eta(y, y') + \mathbf{d}_\zeta(z, z'), t) + \tilde{\beta}(\mathbf{d}_\eta(y, y') + \mathbf{d}_\zeta(z, z'), t) \\ &\quad + \beta_\zeta(\mathbf{d}_\eta(y, y') + \mathbf{d}_\zeta(z, z'), t) + \hat{\gamma}(\|v - v'\|_\infty) \\ &\quad + \tilde{\gamma}_v(\|v - v'\|_\infty) \\ &\leq \beta(\mathbf{d}(x, x'), t) + \gamma(\|v - v'\|_\infty), \quad (\text{A.3}) \end{aligned}$$

where $\beta \in \mathcal{K}\mathcal{L}$ and $\gamma \in \mathcal{K}_\infty$ are defined as following:

$$\begin{aligned} \beta(r, t) &= \hat{\beta}(r, t) + \tilde{\beta}(r, t) + \beta_\zeta(r, t), \\ \gamma(r) &= \hat{\gamma}(r) + \tilde{\gamma}_v(r). \end{aligned}$$

Hence, the overall system Σ of the form (4.2) is δ_3 -ISS with respect to v .

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